

2026 International Energy and
Environment Conference

A Study on Enhancing the Thermal Management System Control of Fuel Cell Hybrid Electric Vehicles Using the Sparrow Search Algorithm

Department of Mechanical and Electro-Mechanical Engineering
National Sun Yat-sen University, Kaohsiung, 804201, Taiwan

Presenter: Prof. Jenn-Kun Kuo

Date: 07-09 September 2026

Hydrogen and Fuel Cell Laboratory
氫能與燃料電池實驗室

Outline

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- Background
- Literature review
- Research Motivation and objectives

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- Vehicle Structure
- Subsystem Introduction
- Surrogate Model Development
- SSA and Fuzzy PI Control

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- Vehicle System Performance
- PI Controller Optimization at Different Speeds
- Fuzzy Gain-Scheduling Control Results
- Comparison of Thermal Management Strategies

5

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Reference

PEMFC THERMAL MANAGEMENT: RESEARCH EVOLUTION

From component-level control to vehicle-level intelligent optimization

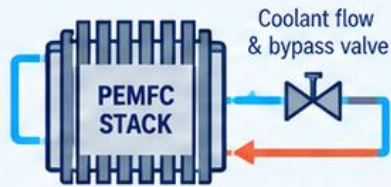
THERMAL MANAGEMENT MODELING & CONTROL

FROM COMPONENT CONTROL TO VEHICLE INTEGRATION

2010 · Hu et al. [6]

Incremental Fuzzy Control

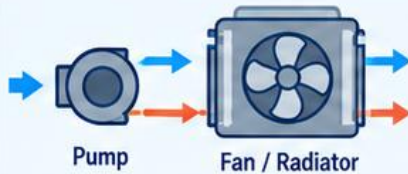
- Coolant flow + bypass valve
- 343 K; max deviation 1.3 K
- Better disturbance rejection than PI



2015 · Han et al. [2]

75-kW Dynamic Cooling Model

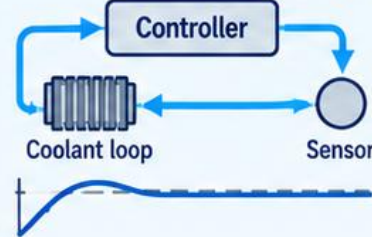
- Pump, fan and bypass strategies
- Fan dominates parasitic power
- Temperature + energy co-optimization



2015 · Cheng et al. [3]

Fuel-Cell Bus Control

- Feedforward + feedback
- Vehicle-test validation
- Coolant maintained near target



2020 · Xu et al. [1]

Integrated Vehicle Thermal Model

- Stack + intake air + traction motor
- Coupled vehicle-level management



CURRENT RESEARCH FRONTIER

 Vehicle-level multi-source thermal coupling

 Temperature-parasitic energy co-optimization

 Intelligent adaptive control

 Variable-load and real-vehicle validation

INTELLIGENT OPTIMIZATION

FROM ALGORITHM DEVELOPMENT TO CONTROL APPLICATION

2020 · Xue & Shen [4]

Sparrow Search Algorithm (SSA)

- Producer, scrounger and aware roles
- Global exploration + local exploitation



2022 · Xu et al. [5]

SSA-Optimized PID

- Faster temperature tracking
- Better dynamic response
- Stronger disturbance rejection

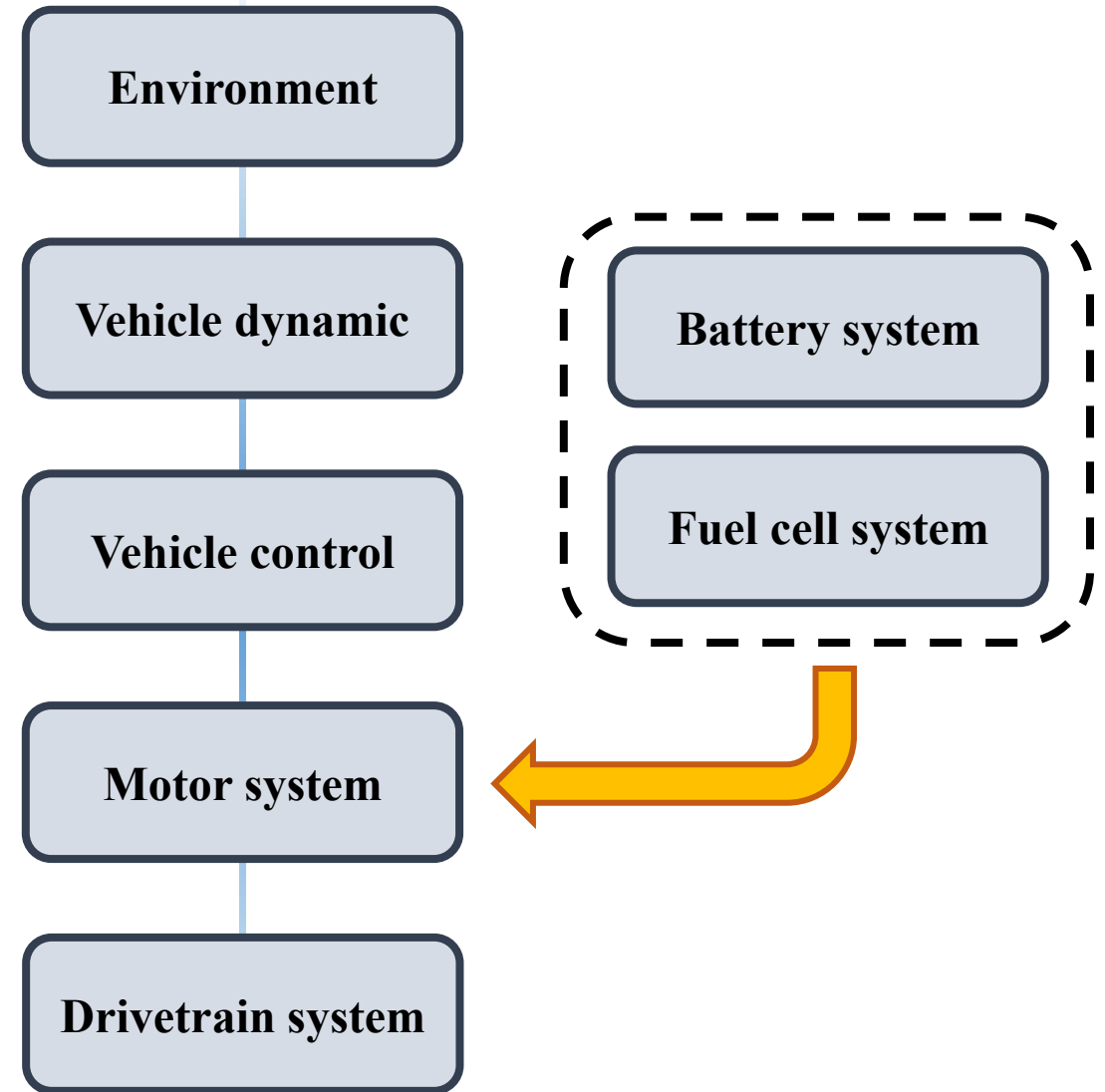
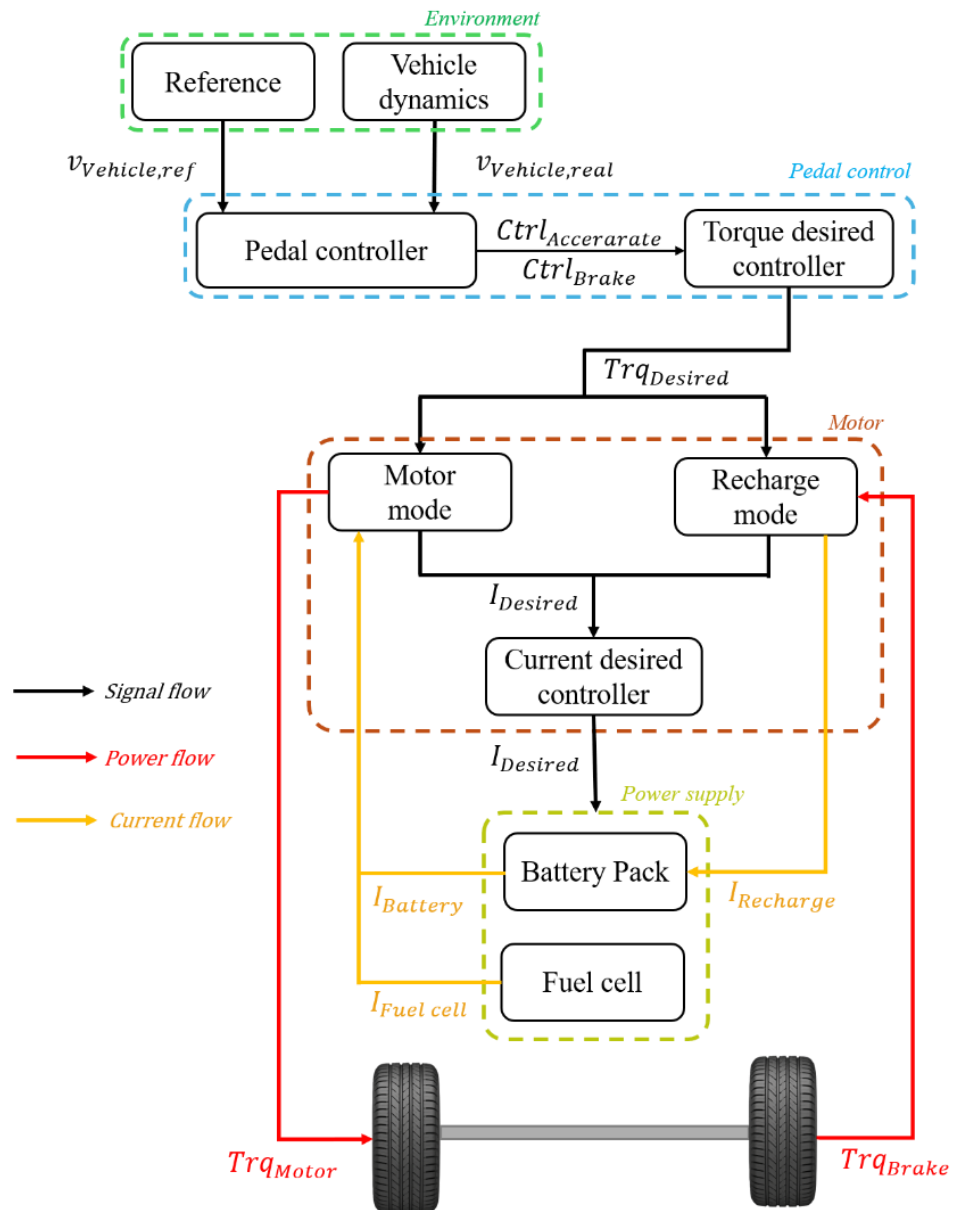


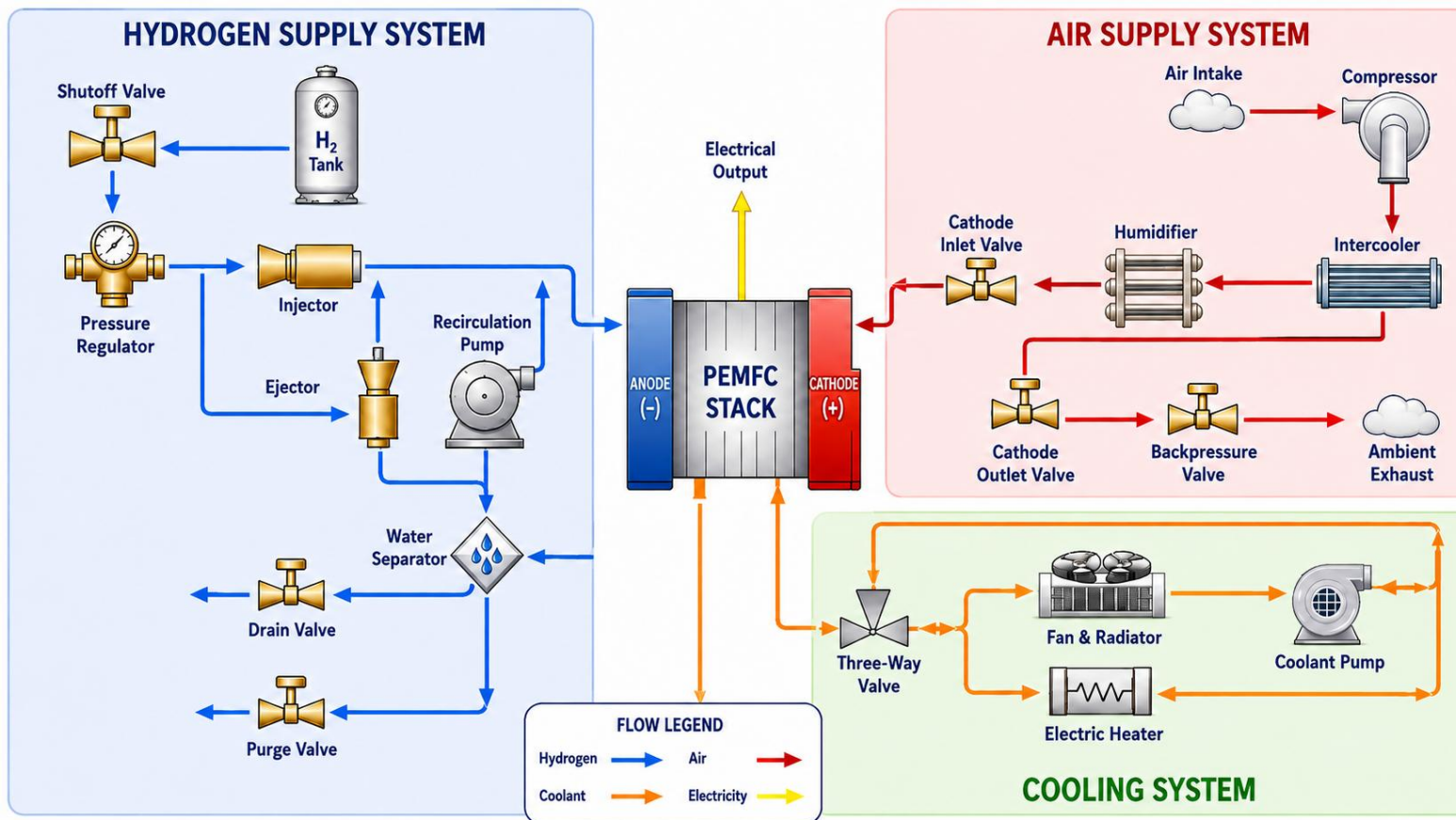


Hyundai Elec City Fuel Cell		
Components	Value	Unit
Length	10995	mm
Width	2490	mm
Height	3400	mm
Gross Vehicle Weight	16,000	kg
Wheel Radius	0.47	m
Drive	Rear-wheel drive	-

This study investigates the thermal management control of a fuel cell electric bus under varying vehicle speeds and thermal loads. Since a **fixed-gain PI controller** cannot fully accommodate low, medium, and high-speed operating conditions, it may result in **insufficient cooling performance** or excessive **parasitic power consumption** from the coolant pump and radiator fan.

Therefore, this study divides the vehicle operating range into several speed regions and applies the **Sparrow Search Algorithm** to optimize the PI parameters for each region. **Fuzzy logic** is then introduced to **schedule the controller gains smoothly** according to vehicle speed. The objective is to maintain **stable stack temperature** while reducing cooling-system parasitic power consumption and **improving the overall energy efficiency** of the fuel cell electric bus.





Anode inlet

Hydrogen Tank	Shutoff valve
Pressure regulator	Injector

Anode outlet

Purge valve	Drain valve
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Anode Recirculation

Water separator	Recirculation pump	Ejector
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Cathode inlet

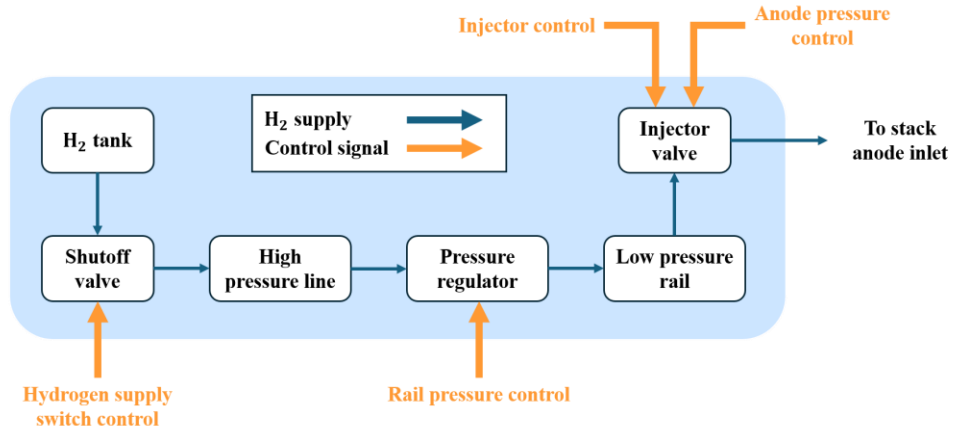
Compressor	Intercooler	Isolation valve
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Cathode outlet

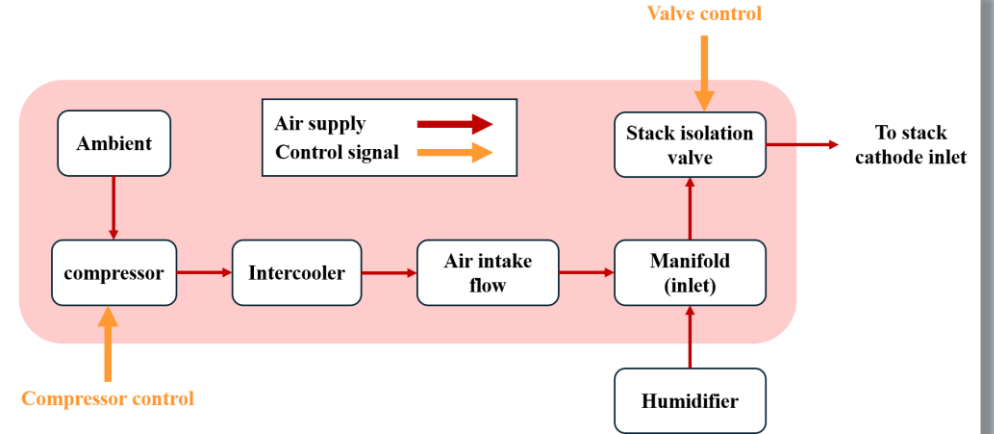
Humidifier	Backpressure valve	Isolation valve
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Cooling system

Coolant pump	Electric heater
Radiator	Fan



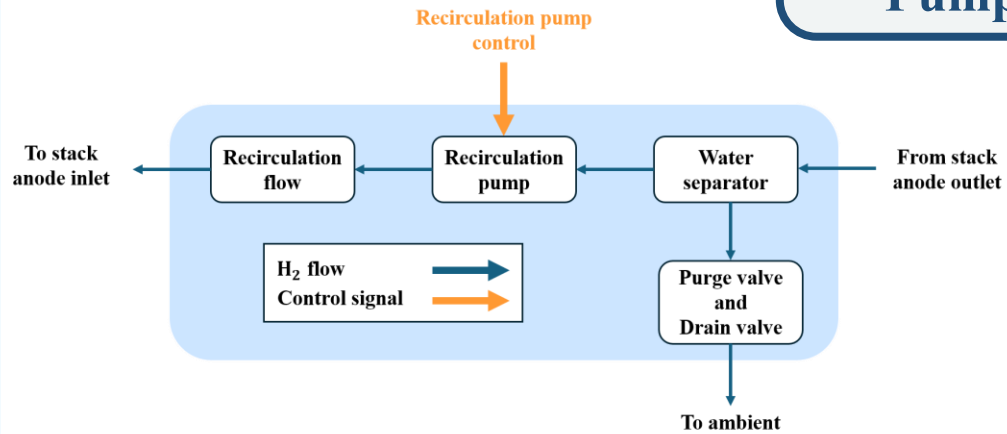
Hydrogen supply system



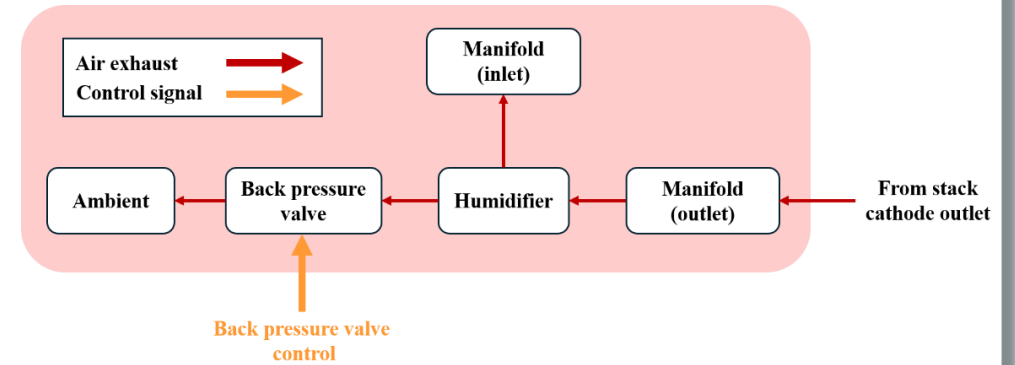
Air supply system

Compressor
&
Pump

Valve

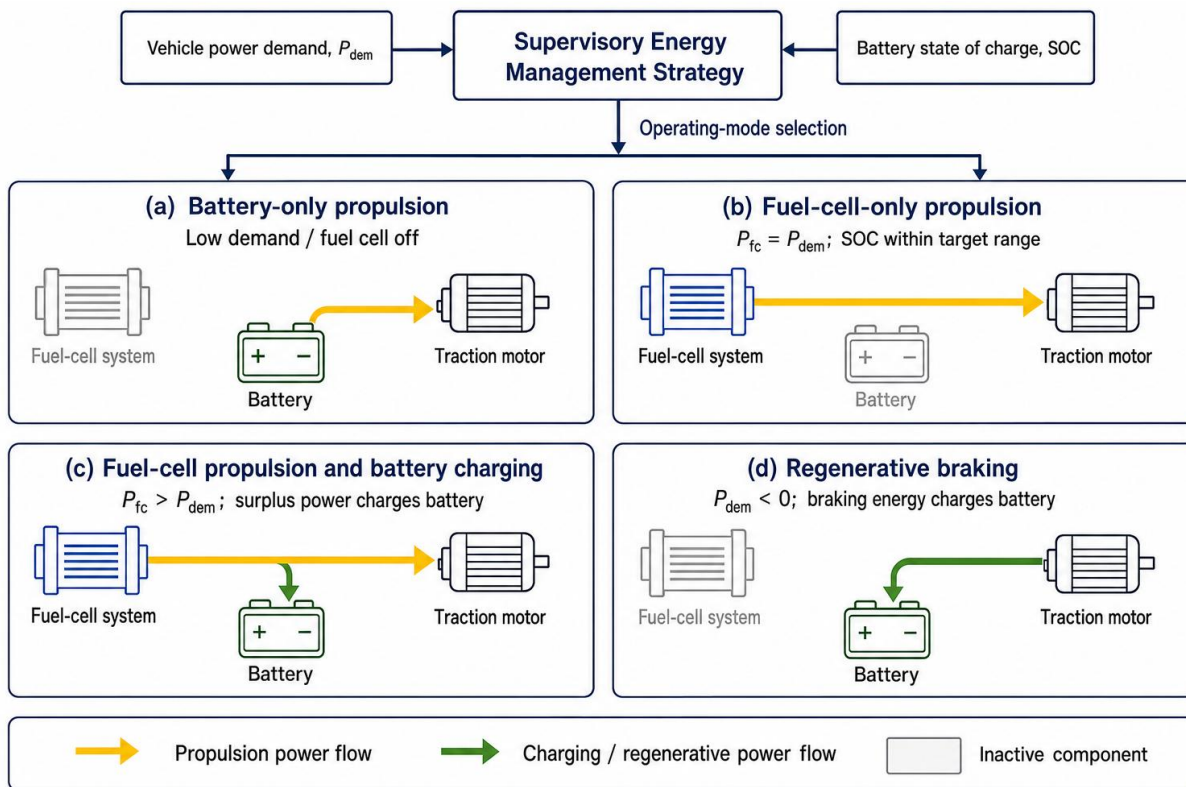


Hydrogen exhaust system



Air exhaust system

Vehicle Control

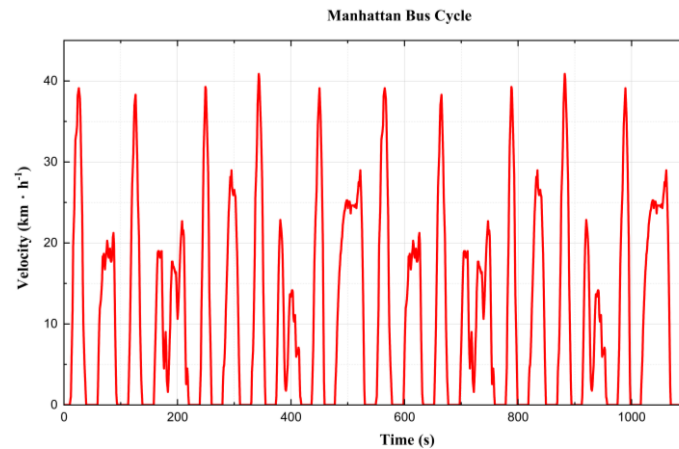


- **Start-up** : The lithium battery provides the initial traction power because the fuel cell requires a short period to establish stable electrochemical operation. This prevents delayed motor response during vehicle launch.
- **Acceleration** : As the traction power demand increases, the fuel cell and lithium battery operate together to supply the motor. The battery provides additional power to compensate for the slower dynamic response of the fuel cell.
- **Cruising** : Under relatively steady driving conditions, the fuel cell supplies most of the motor power. When the battery SOC is low and surplus fuel cell power is available, part of the energy can be used to recharge the battery.
- **Deceleration** : During braking or vehicle deceleration, the motor operates in regenerative mode. The recovered kinetic energy is converted into electrical energy and stored in the lithium battery for later use.

Environment

Manhattan Bus Cycle

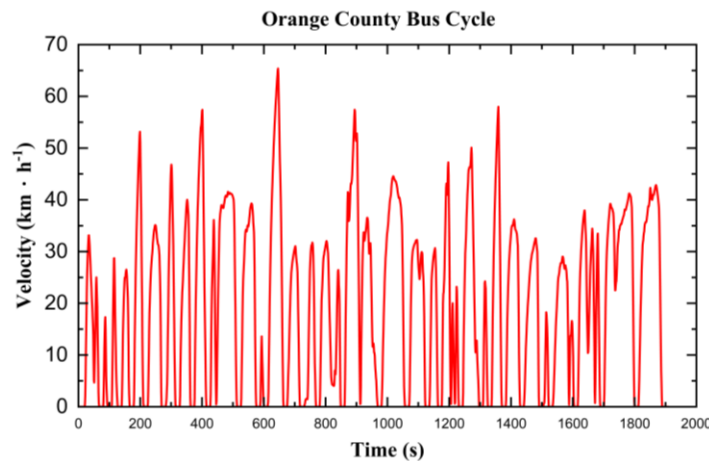
MBC is a low-speed urban bus cycle with frequent stops and accelerations. It represents congested city traffic.



Travel time	1089 s	Average speed	11.0 km/h
Distance	3.33 km	Maximum speed	40.88 km/h

Orange County Bus Cycle

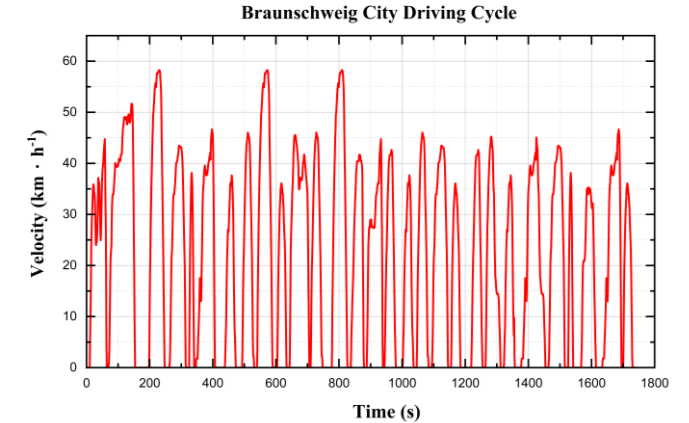
OCBC is a bus driving cycle with frequent speed variations and moderate-to-high speeds.



Travel time	1909 s	Average speed	19.31 km/h
Distance	10.53 km	Maximum speed	65.98 km/h

Braunschweig City Driving Cycle

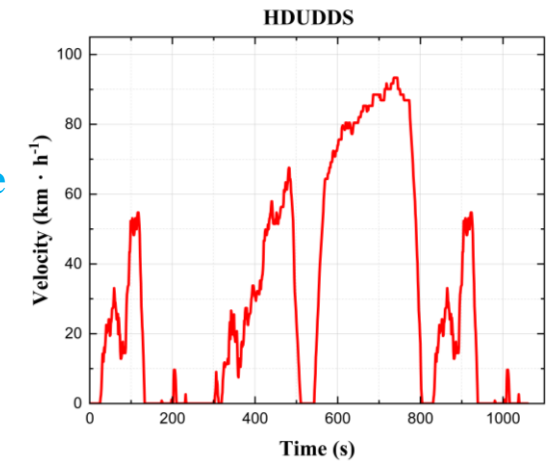
BCDC is an urban bus cycle with repeated acceleration, deceleration, and stop-and-go operation. It covers a wider speed range than MBC.



Travel time	1740 s	Average speed	22.53 km/h
Distance	10.88 km	Maximum speed	58.26 km/h

Heavy-Duty Urban Dynamometer Driving Schedule

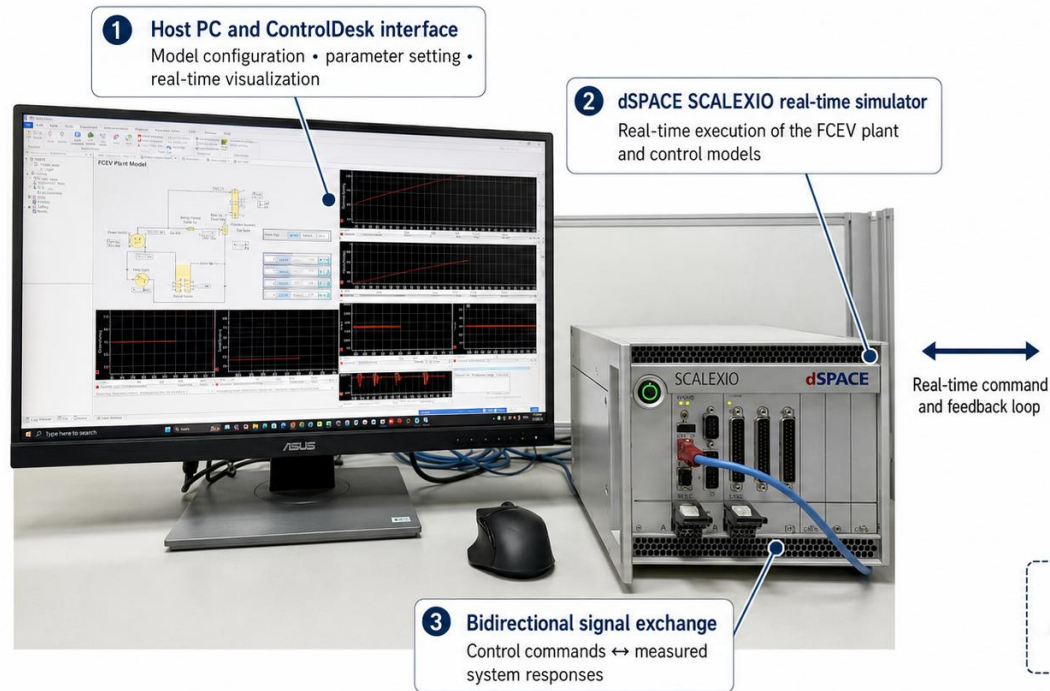
HDUDDS is a heavy-duty urban driving cycle combining stop-and-go traffic with high-speed sections. It produces large variations in vehicle load and power demand.



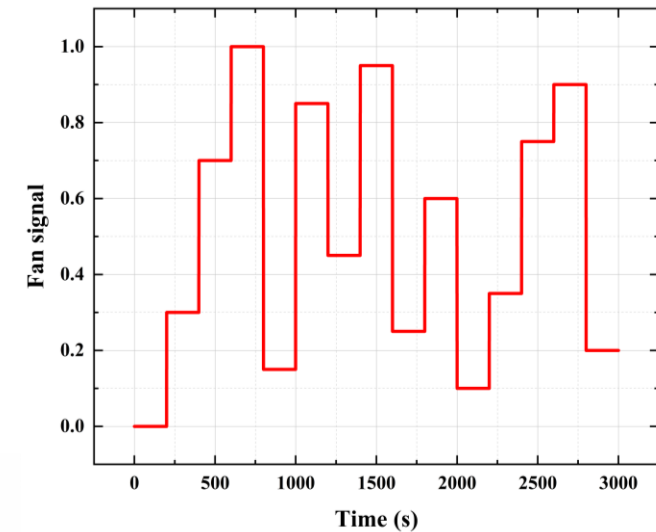
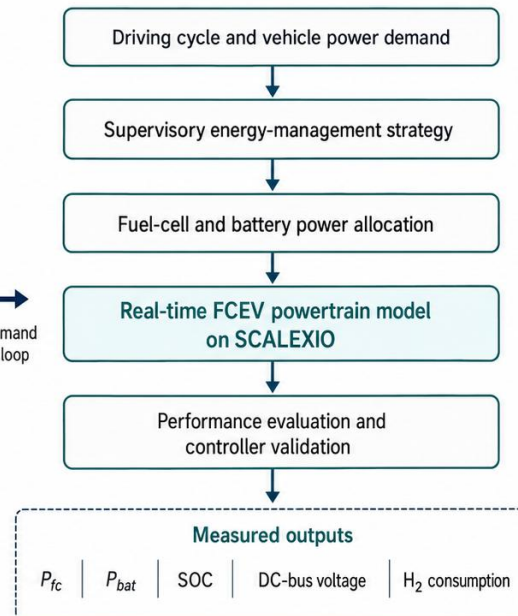
Travel time	1060 s	Average speed	30.35 km/h
Distance	8.93 km	Maximum speed	93.34 km/h

Surrogate Model (Agent model)

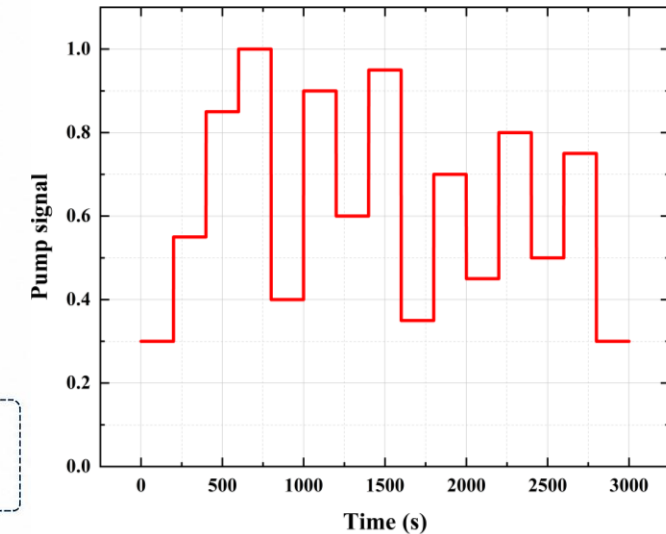
- Training data for the surrogate models were collected using the **dSPACE SCALEXIO real-time platform**. Stepwise fan and pump commands were applied across their operating ranges, while the corresponding coolant temperatures and system responses were recorded through ControlDesk. The measured input–output data were subsequently used for **system identification and model validation**.



Real-Time HIL Research Model

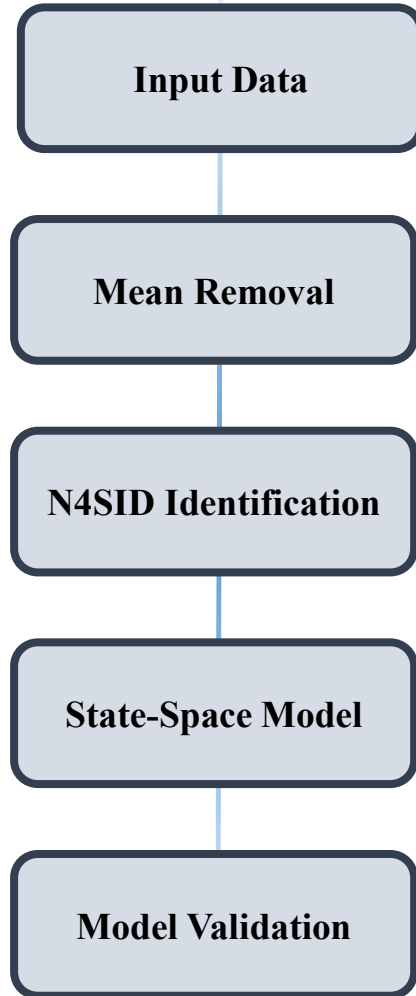


Fan Excitation Signal for Data Collection



Pump Excitation Signal for Data Collection

Surrogate model



- System identification is used to construct a low-order surrogate model from input – output data, reducing the computational cost of controller optimization while preserving the dominant thermal dynamics.

Key equation

Identified State-Space Model

- $x(k+1) = Ax(k) + Bu(k) + Ke(k)$
- $y(k) = Cx(k) + Du(k) + e(k)$

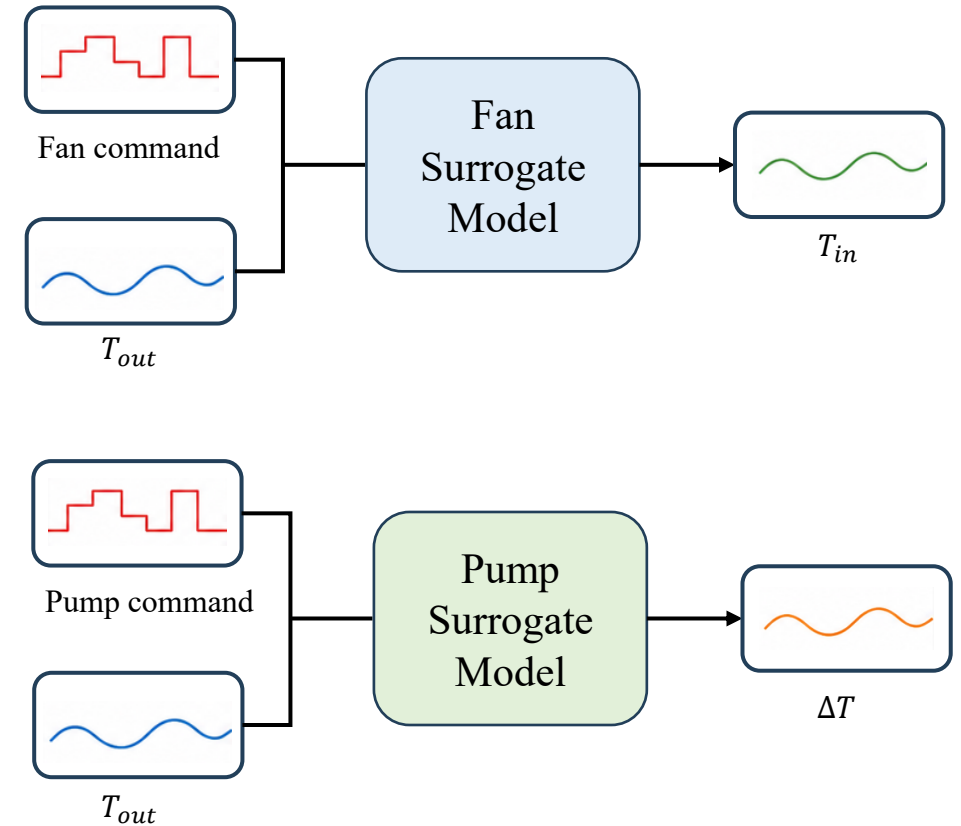
N4SID Identification Relation

- $Y_f = \Gamma_f X_k + H_f U_f + G_f E_f$

Model Accuracy Evaluation

- $fit = 100(1 - \frac{\|\hat{y} - y\|}{\|y - \text{mean}(y)\|})$

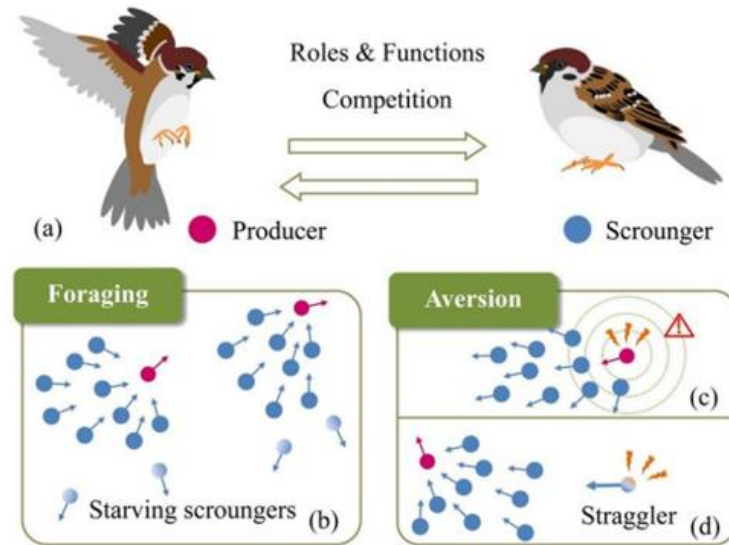
Model I/O



Sparrow Search Algorithm (SSA)

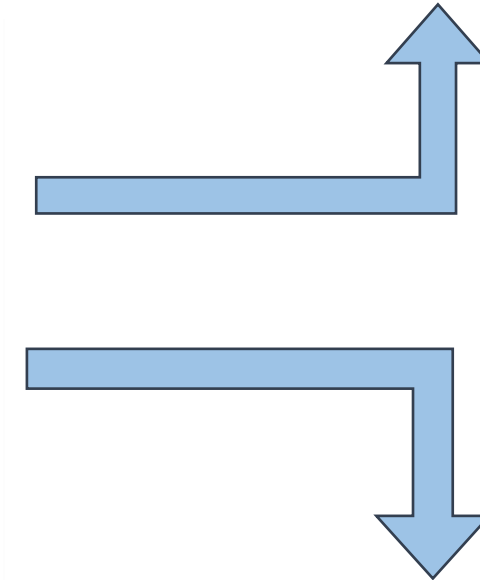
- Producer**

$$X_{i,j}^{t+1} = \begin{cases} X_{i,j}^t \cdot \exp\left(-\frac{i}{\alpha \cdot iter_{max}}\right), R_2 < ST \\ X_{i,j}^t + Q \cdot L, R_2 \geq ST \end{cases}$$



- Scrounger**

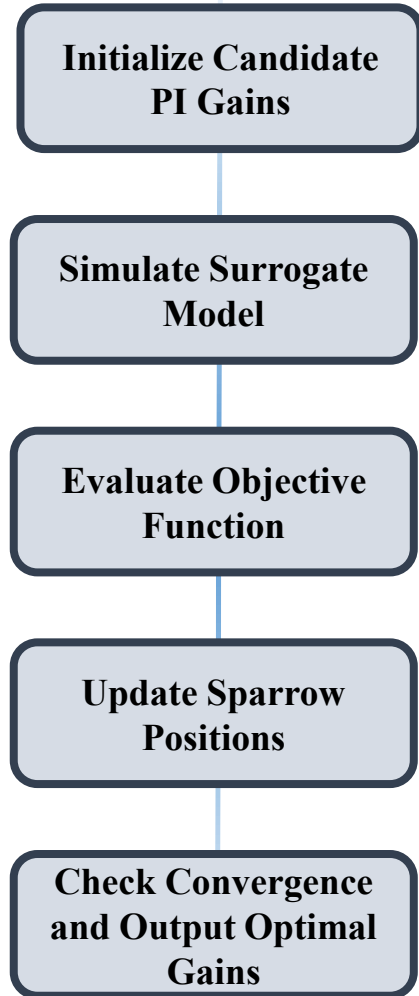
$$X_{i,j}^{t+1} = \begin{cases} Q \cdot \exp\left(-\frac{X_{worst}^t - X_{i,j}^t}{i^2}\right), i > \frac{n}{2} \\ X_P^{t+1} + |X_{i,j}^t - X_P^{t+1}| \cdot A^+ \cdot L, otherwise \end{cases}$$



- Aware Sparrows**

$$X_{i,j}^{t+1} = \begin{cases} Q \cdot \exp\left(-\frac{X_{worst}^t - X_{i,j}^t}{i^2}\right), i > \frac{n}{2} \\ X_P^{t+1} + |X_{i,j}^t - X_P^{t+1}| \cdot A^+ \cdot L, otherwise \end{cases}$$

Sparrow Search Algorithm (SSA)



$$J_{fan} = J_{T,high} + J_{T,low} + J_u + J_{\Delta u} + J_{sat} + J_{ss}$$

Temperature
Tracking
Performance

Control
Effort and
Stability

$$J_{pump} = J_{\Delta T,high} + J_{\Delta T,low} + J_u + J_{\Delta u} + J_{sat} + J_{ss}$$

Number of sparrows	50
Maximum iteration	70
Search dimension	2
Final selection criterion	Minimum fitness value
Initial PI gains	$K_p: 0.05$ $K_i: 0.005$
Search range of PI gains	$K_p \in [0, 0.2]$ $K_i \in [0, 0.01]$

Fuzzy Control

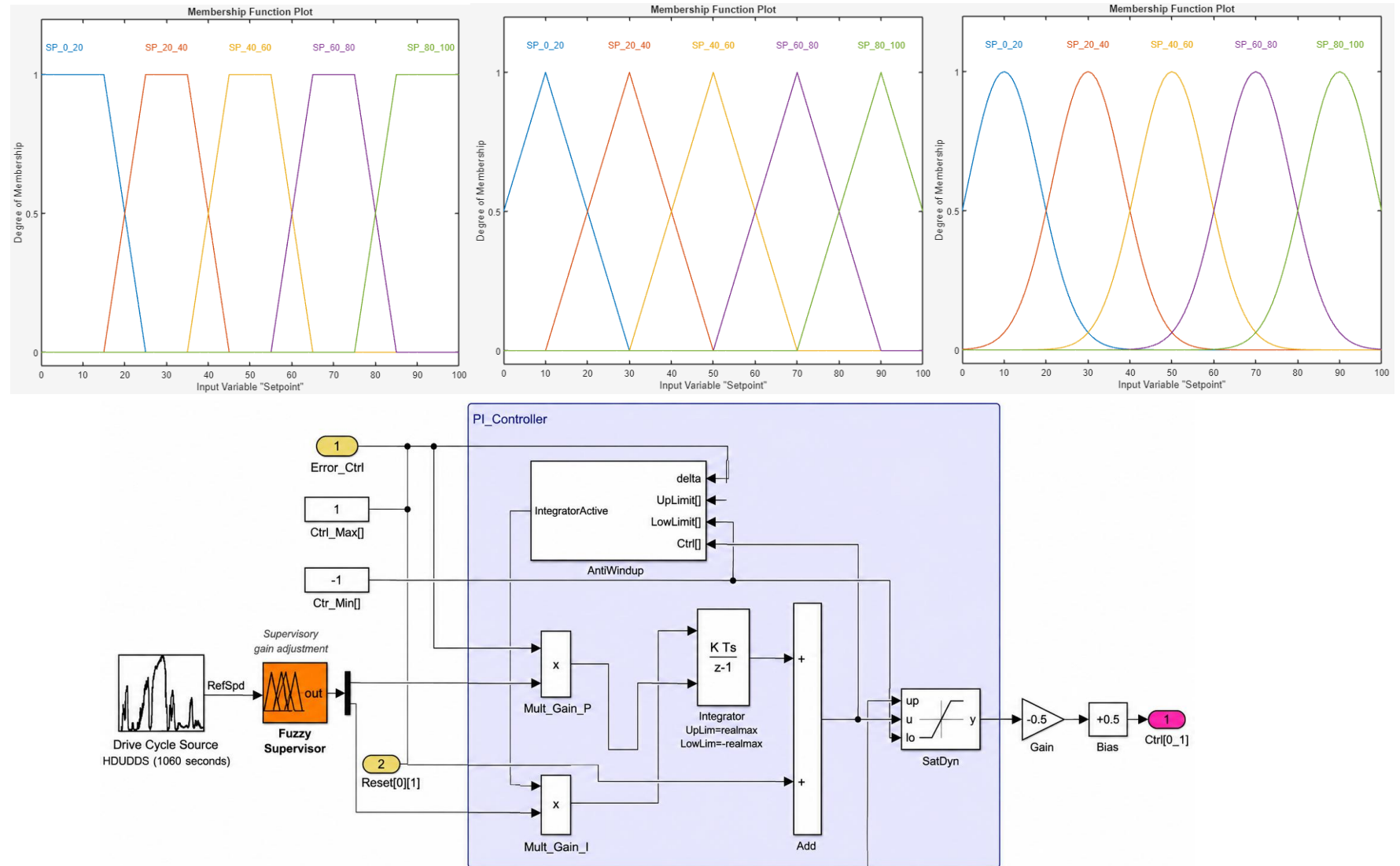
Vehicle Speed Input

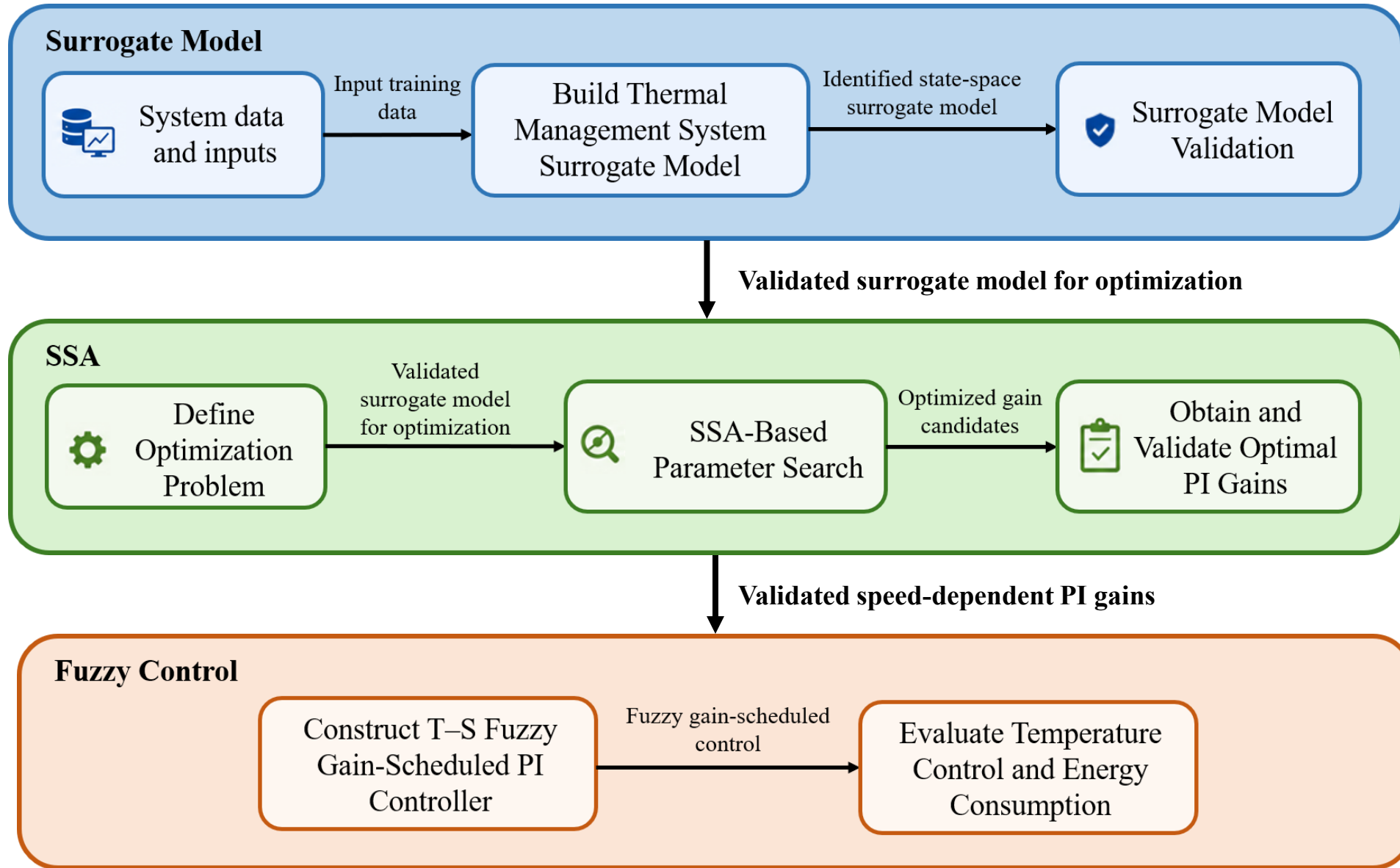
Membership Calculation

Fuzzy Rule Evaluation

PI Gain Scheduling

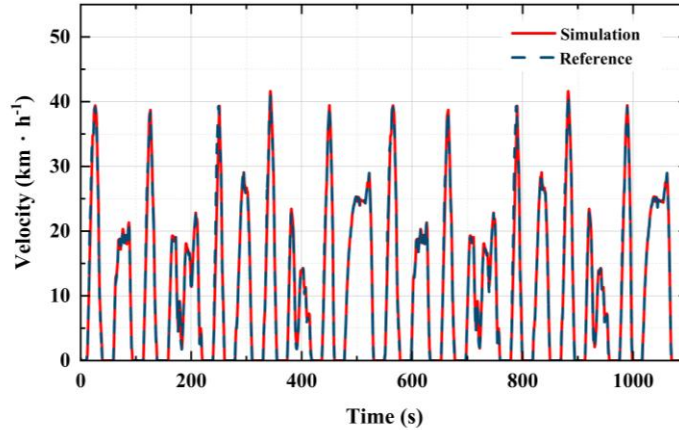
Fan and Pump PI Control



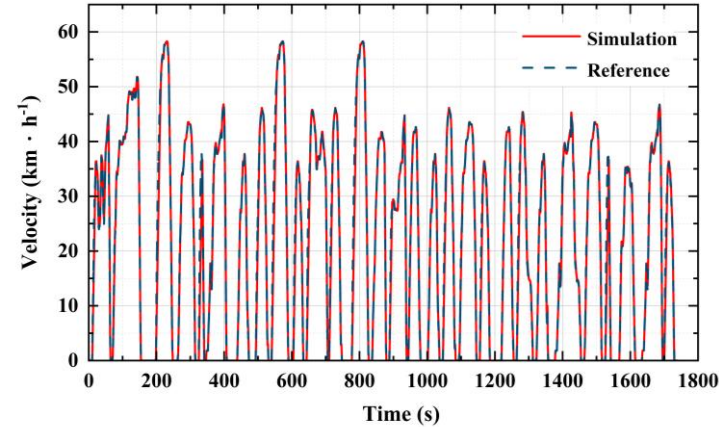


Test Cycle Verification

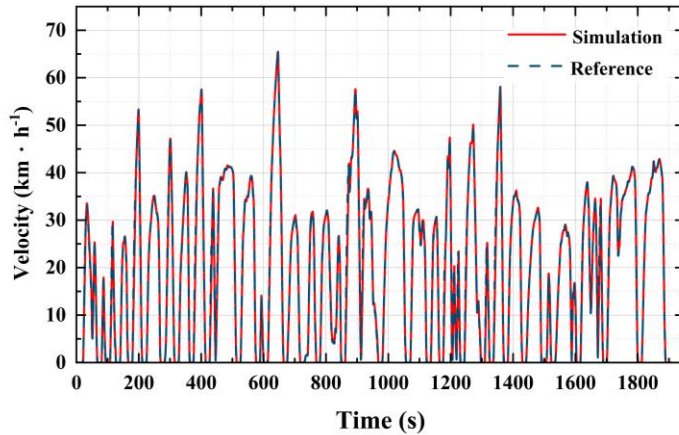
Manhattan Bus Cycle (MBC)



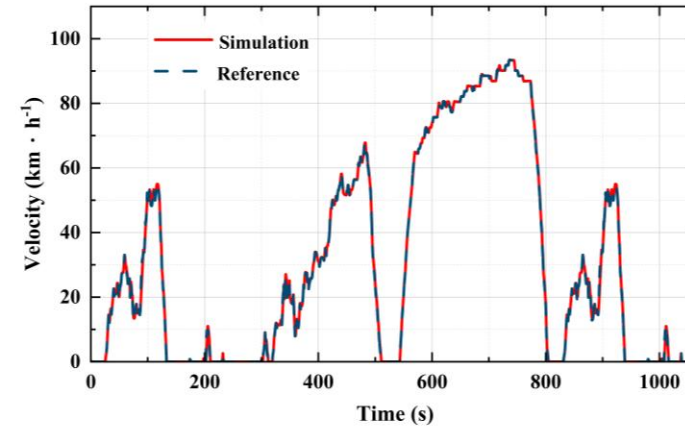
Braunschweig City Driving Cycle (BCDC)



Orange County Bus Cycle (OCBC)



HDUDDS

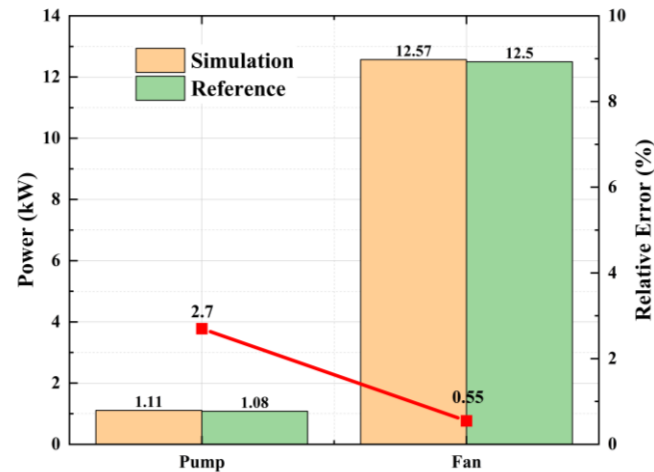
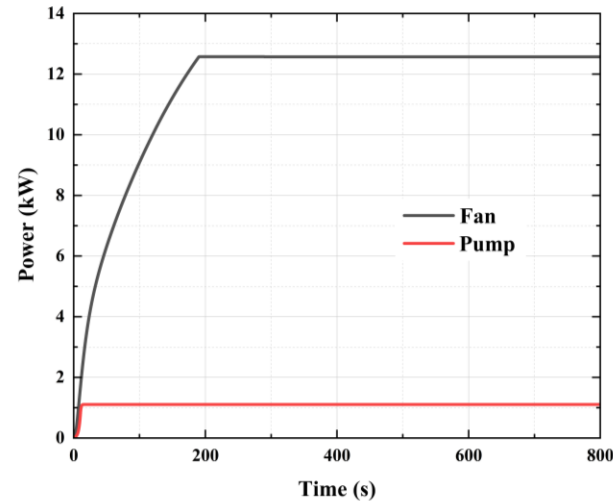


The four driving cycles provide a comprehensive evaluation of the vehicle model under different speed ranges and transient conditions. The simulated vehicle speed closely follows the reference profile in MBC, BCDC, OCBC, and HDUDDS [7], including frequent stop-and-go operation and high-speed variations. These results confirm the model ability to accurately reproduce vehicle speed dynamics under various driving conditions.

[7] A. Łebkowski, Studies of Energy Consumption by a City Bus Powered by a Hybrid Energy Storage System in Variable Road Conditions. Energies 12(5) (2019) 951.

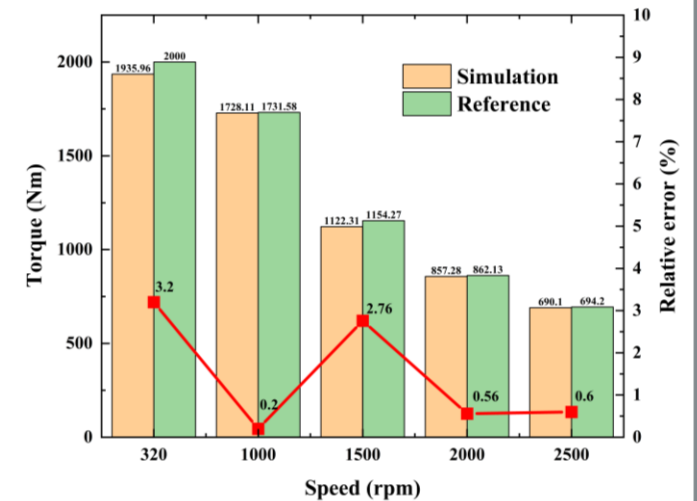
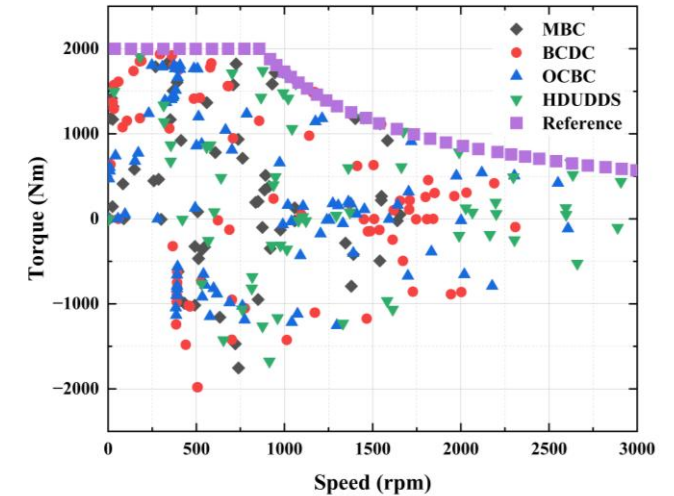
System Verification

The fan and pump power models were validated under a total fuel cell output of 180 kW. The simulated pump and fan powers were 1.11 and 12.57 kW, with relative errors of 2.70% and 0.55%, confirming good agreement with the reference values.



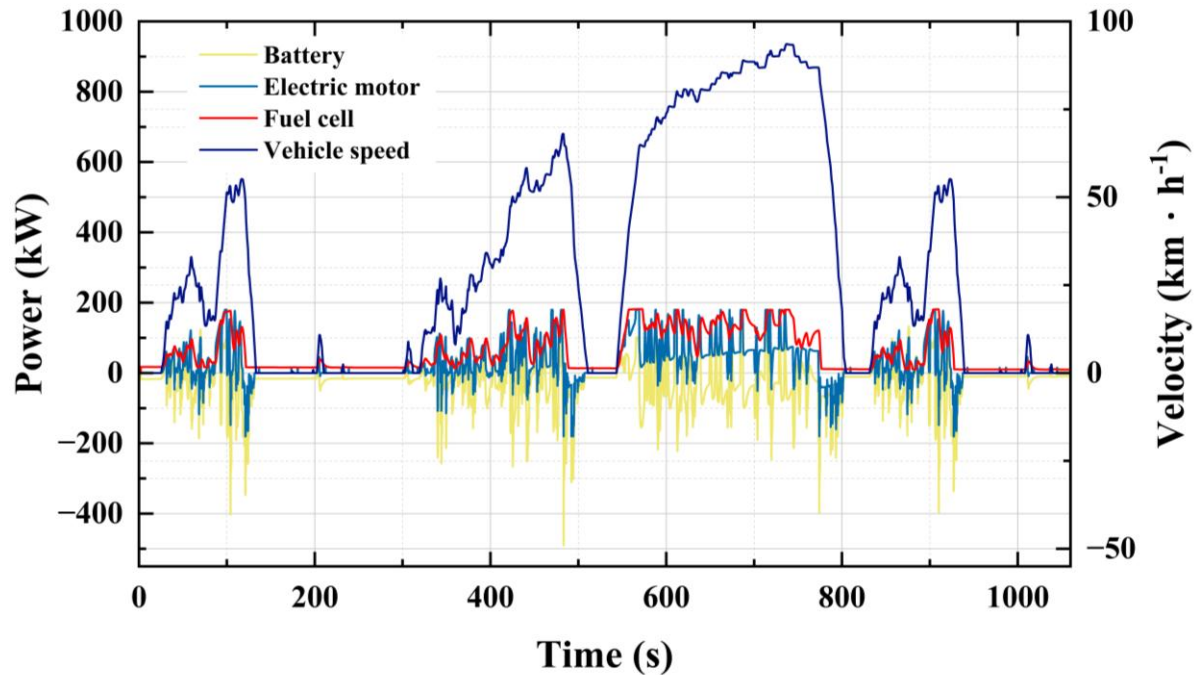
- [8] Y. Kim, J. Kim, and K. Min, Analysis of power consumption on BOP system in a fuel cell electric bus according to the fuel cell load range. International Journal of Automotive Technology 25(4) (2024) 701-715.

The motor model was validated using four driving cycles. The operating points remained within the reference torque–speed envelope. Relative errors at selected speeds ranged from 0.20% to 3.20%, confirming good agreement with the reference data.

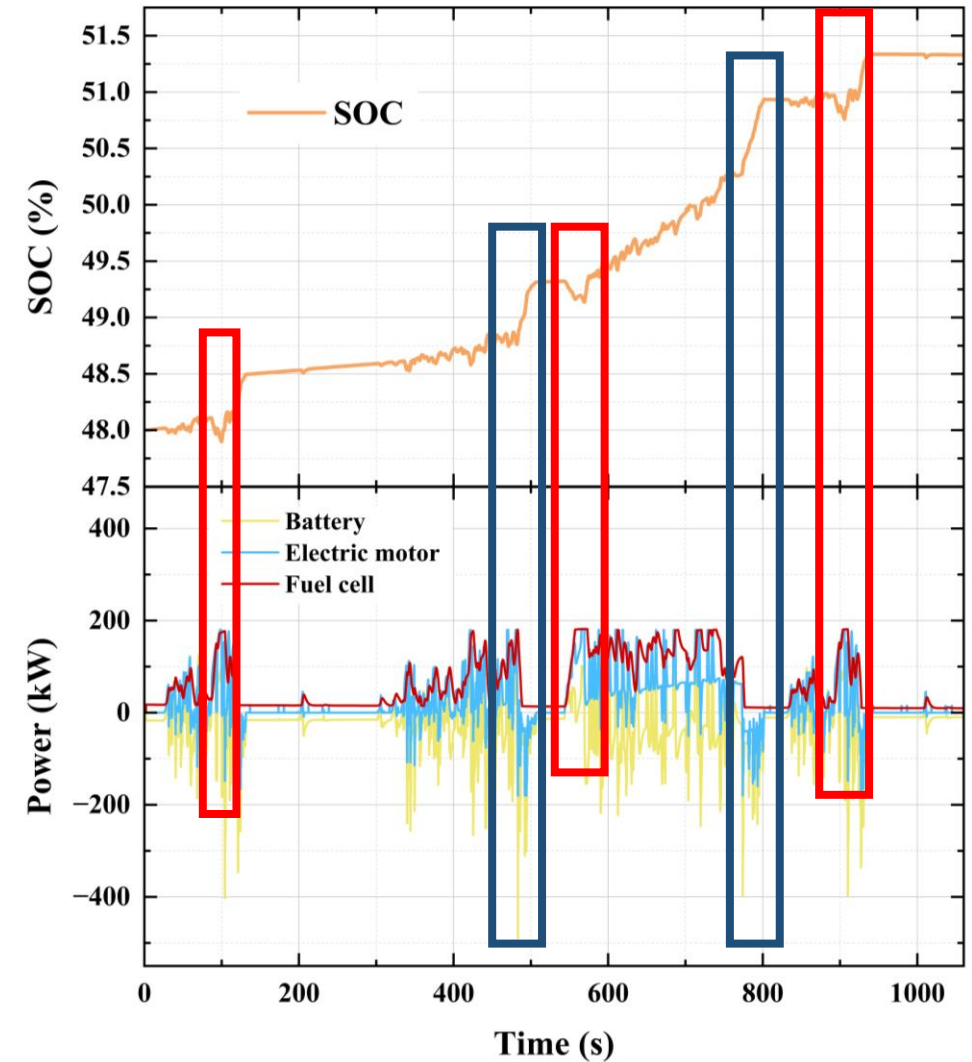


- [9] A. Ritari, J. Vepsäläinen, K. Kivekäs, K. Tammi, and H. Laitinen, Energy Consumption and Lifecycle Cost Analysis of Electric City Buses with Multispeed Gearboxes. Energies 13(8) (2020) 2117.

Vehicle System Performance

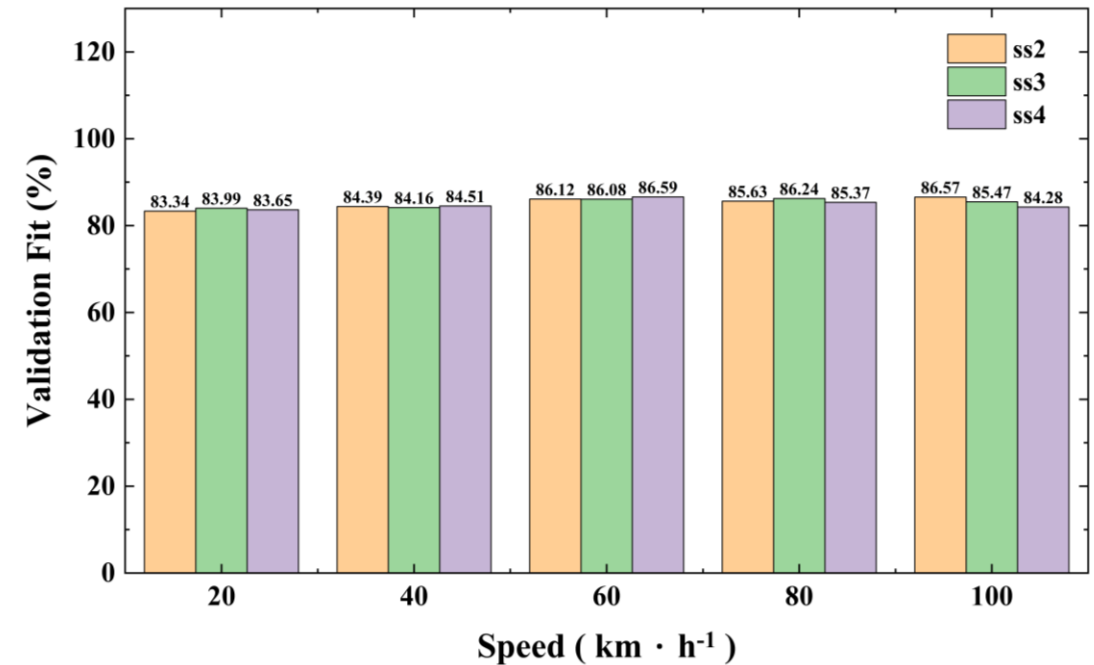
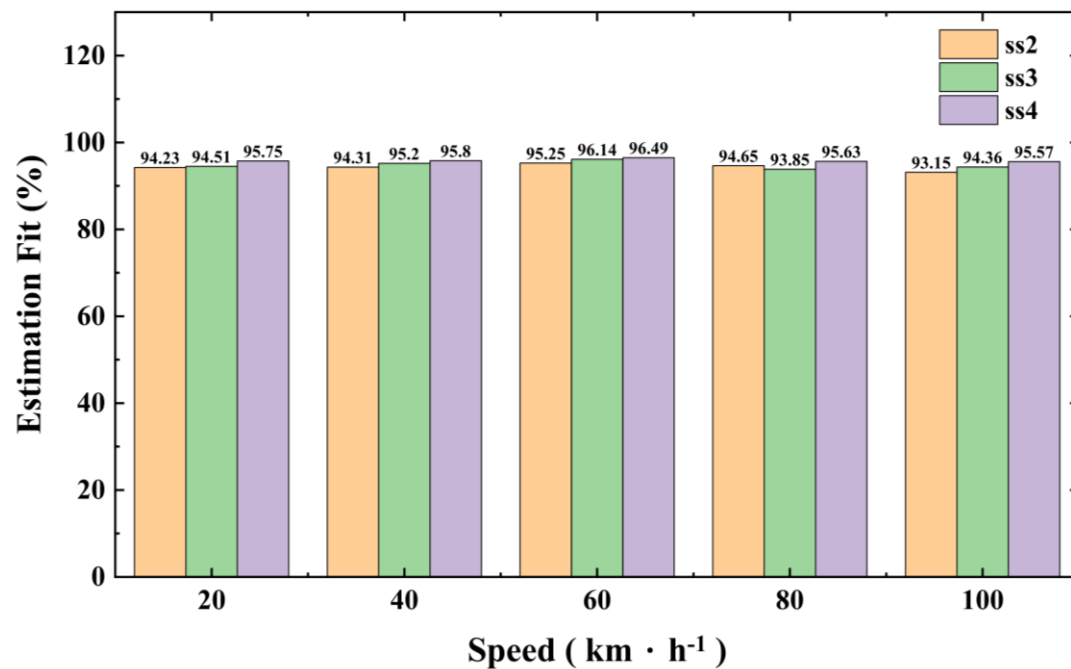


- The traction power demand varies with vehicle speed. The **fuel cell provides the primary power**, while the **battery supports transient load changes** and **absorbs regenerative braking energy** during deceleration.
- The battery SOC increases from approximately 48.0% to 51.3%, indicating that regenerative braking energy and surplus fuel cell power are stored in the battery. The fuel cell and battery jointly satisfy the motor power demand under dynamic driving conditions.



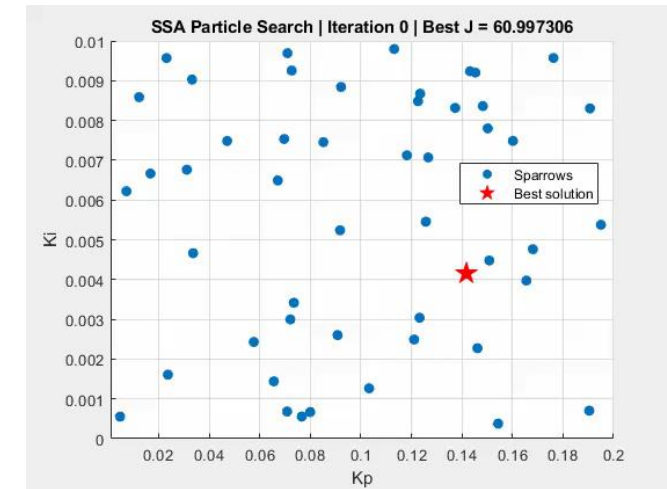
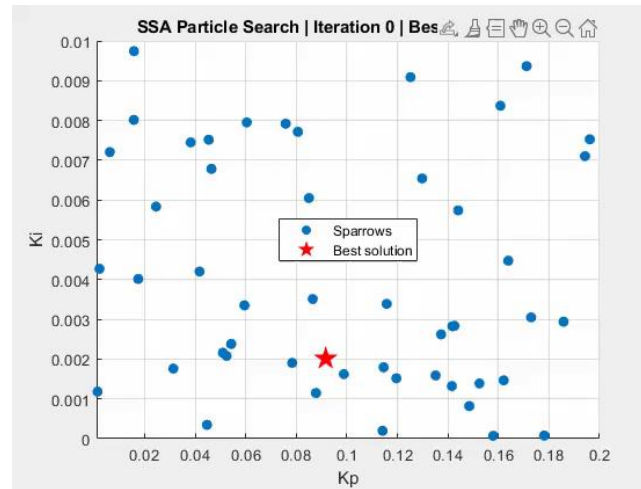
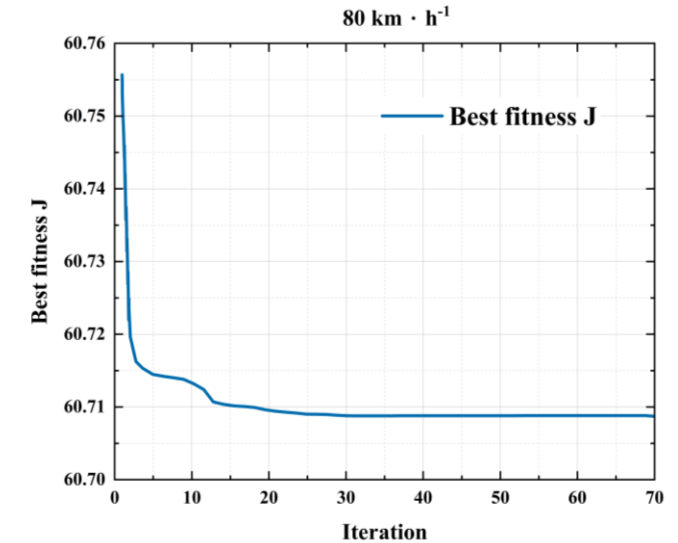
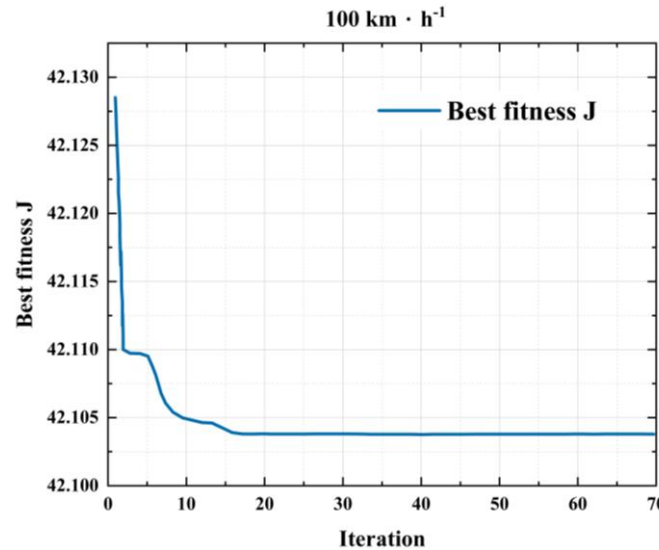
PI Controller Optimization

Second, third, and fourth-order state-space models were evaluated using separate estimation and validation datasets. The estimation fits exceeded 93%, while the validation fits ranged from 83.34% to 86.59%. Since increasing the model order did not consistently improve validation accuracy, the second-order model was selected to balance prediction performance, generalization capability, and computational efficiency.

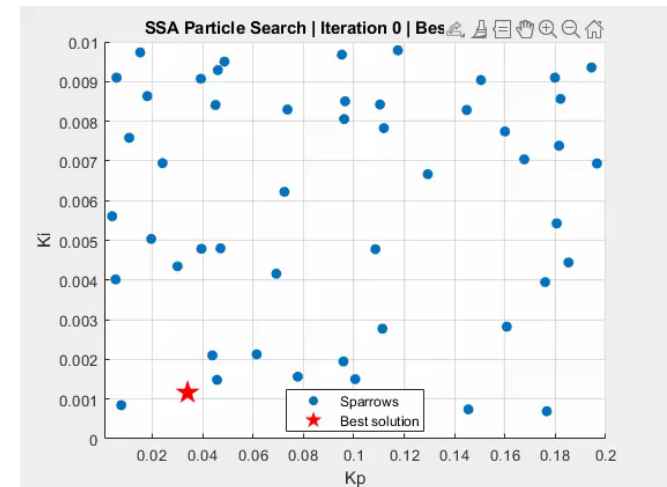
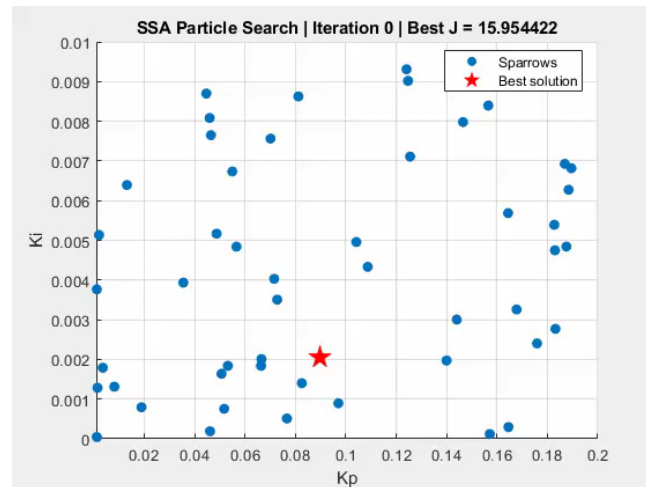
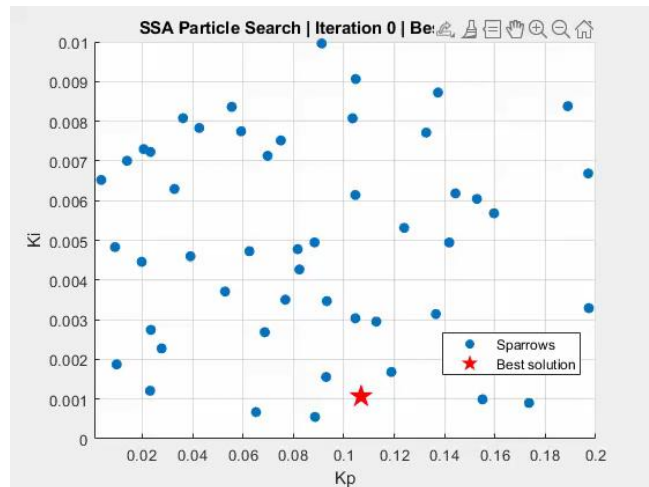
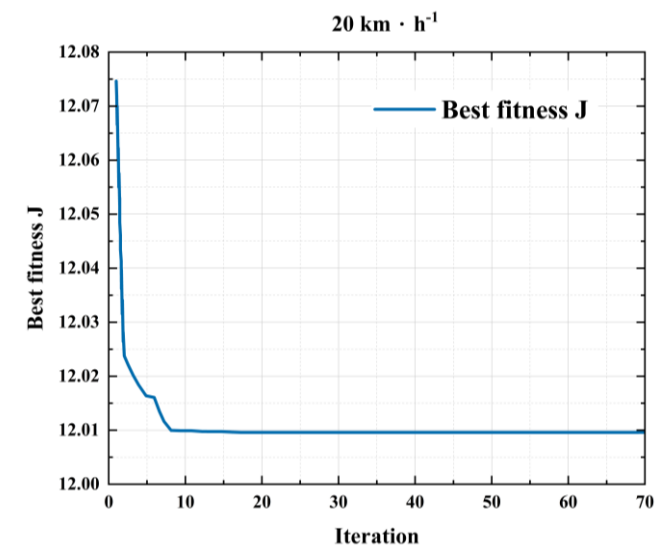
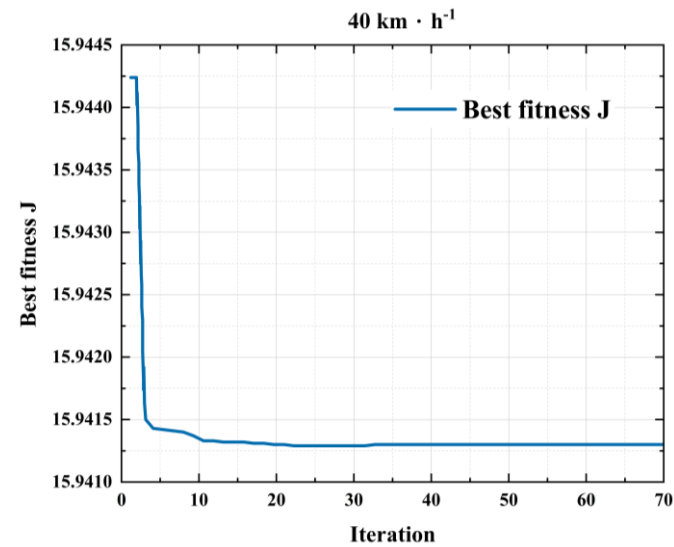
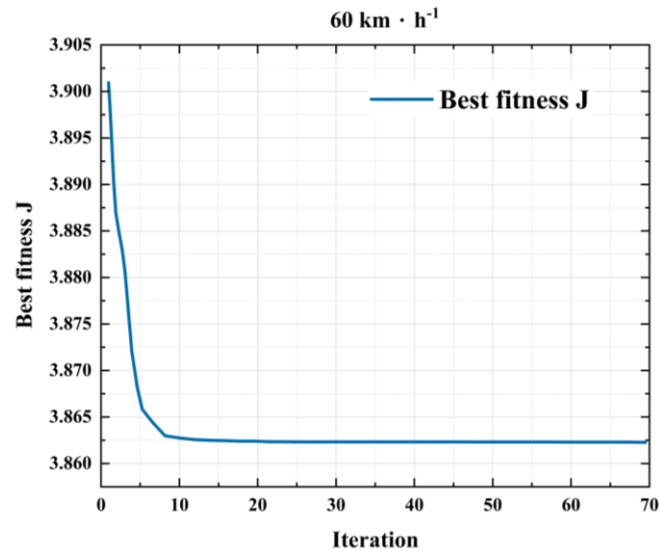


B Sparrow Search Algorithm (SSA) Convergence at Different Vehicle Speeds

The objective function **decreased rapidly** during the early iterations and gradually converged to a stable value at all tested vehicle speeds. Most cases reached convergence within **approximately 10~30 iterations**, indicating that SSA can efficiently and consistently identify suitable PI controller parameters.

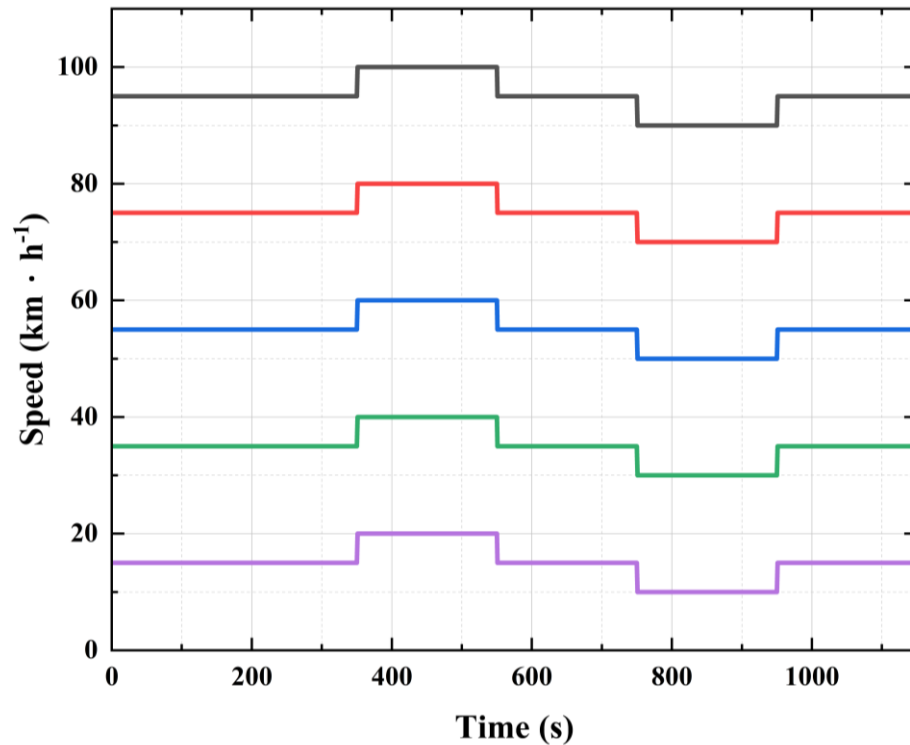


B Sparrow Search Algorithm (SSA) Convergence at Different Vehicle Speeds



C Speed-Scheduled Optimization Test Conditions

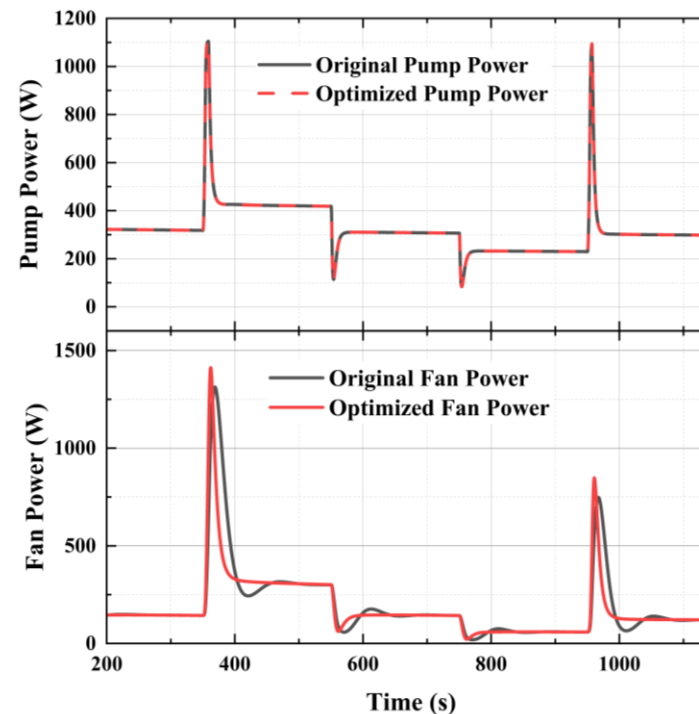
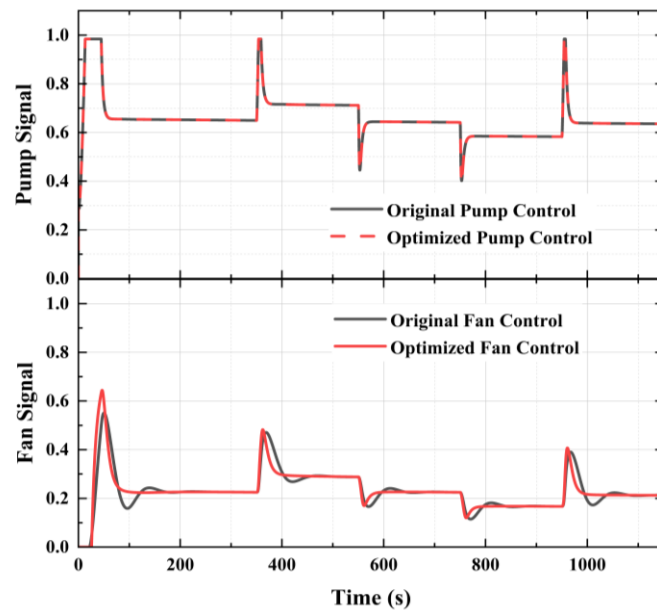
A multi-speed test profile was designed to evaluate the optimized PI controller under different thermal-load conditions. After an initial 200 s acceleration period, each speed was maintained for 150 s to ensure that the thermal response approached a stable operating condition.



Test speeds	100, 80, 60, 40, and 20 km/h
Initial acceleration period	200 s
Duration of each speed segment	150 s
Comparison	Original PI vs. SSA-Optimized PI

D Control Response and Energy Consumption at 100 km/h

- The pump is **controlled by a feedforward** lookup table, so its command remains nearly unchanged after optimization.
- The optimized fan PI controller **reduces control oscillation** and peak duration.
- Unnecessary fan operation is reduced, resulting in a **5.11% decrease** in fan energy consumption.



Control Strategy	Fan Energy Consumption (Wh)	Energy Saving Rtae (%)
Original PI	50.34	—
Optimized PI	47.20	5.11 %

Comparison of Thermal Management Strategies

- FFP-OPI :**

Feedforward Pump + Original PI Fan Control

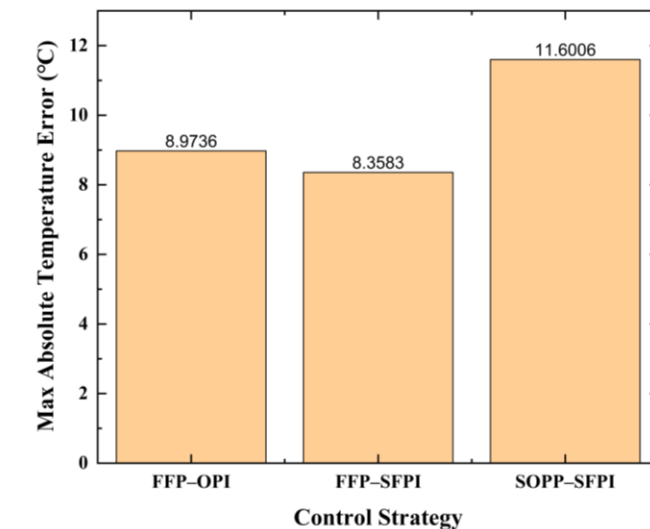
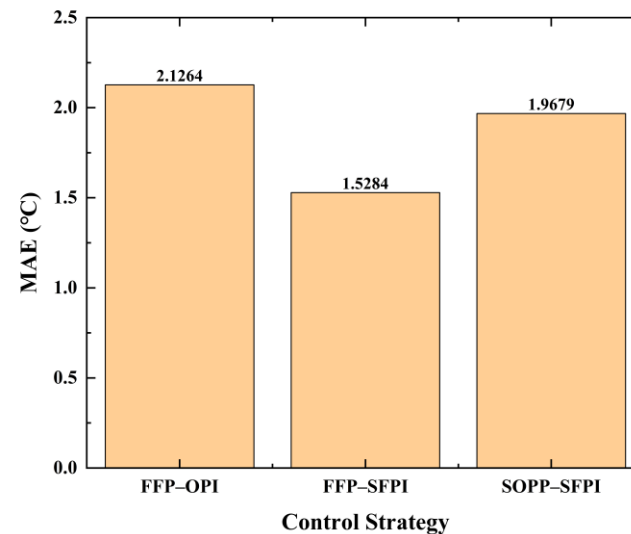
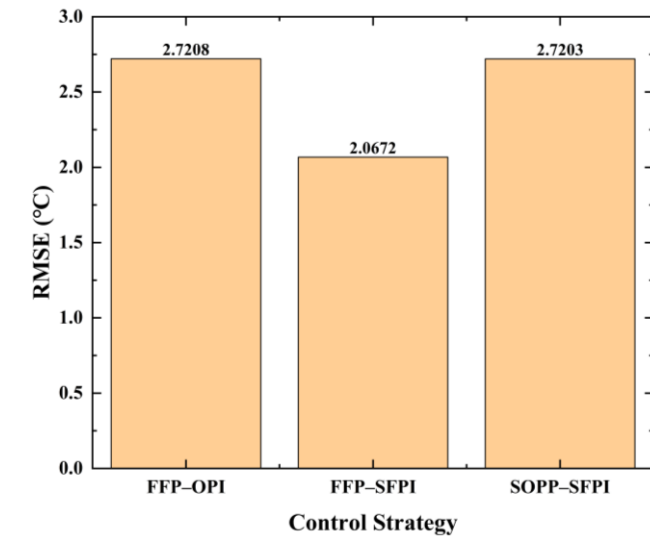
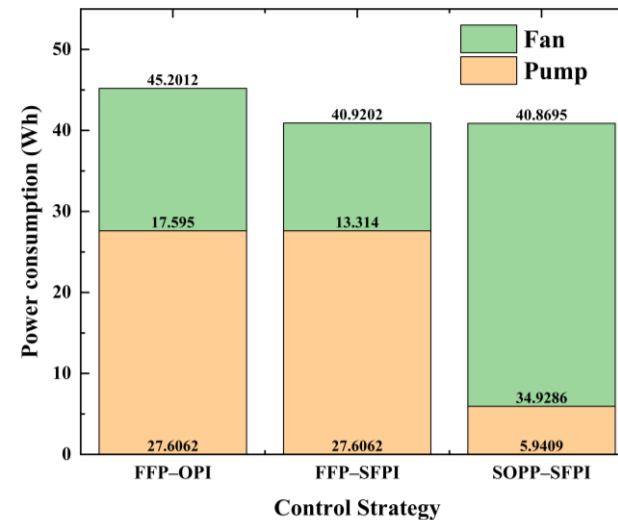
- FFP-SFPI :**

Feedforward Pump + SSA-Optimized Fuzzy
PI Fan Control

- SOPP-SFPI :**

Optimized Pump PI + SSA-Optimized Fuzzy
PI Fan Control

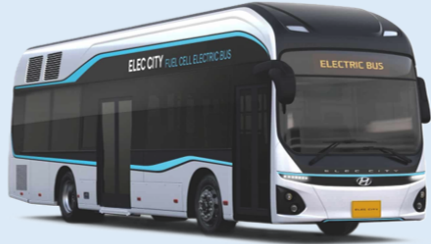
FFP-SFPI provides the best balance between temperature-tracking accuracy and auxiliary energy consumption.



Research Highlights

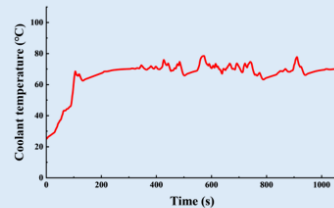
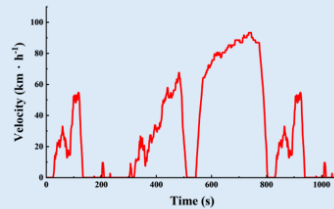
Surrogate-Model-Based SSA Optimization with Fuzzy Gain-Scheduled PI Control for Fuel Cell Bus Thermal Management

1. Research problem



Fuel Cell Bus Thermal Management Challenge

- Thermal load varies with vehicle speed
- Fixed-gain PI control cannot adapt to all operating conditions

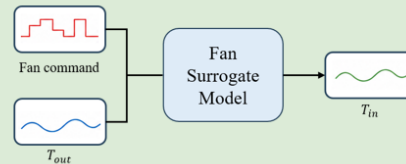


2. Research Methodology

- 1 dSPACE Data Collection
 - Real-time control
 - Data acquisition
 - Fan, pump, and temperature signals



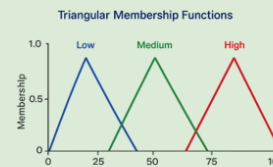
- 2 Surrogate Model Development



- 3 SSA Optimization of PI Parameters
- Search Space (K_p, K_i)
- K_i
 - K_p



- 4 Fuzzy Gain-Scheduled PI Control



3. Performance evaluation

Control Strategy Comparison

- FFP-OPI : Feedforward Pump + Original PI Fan
- FFP-SFPI : Feedforward Pump + SSA-Optimized Fuzzy PI Fan
- SOPP-SFPI : SSA-Optimized Pump PI + SSA-Optimized Fuzzy PI Fan

Evaluation Metrics

- RMSE
- MAE
- Maximum Absolute Temperature Error
- Auxiliary Energy

4. Key outcomes

Best Strategy: FFP-SFPI

Total Auxiliary Energy

9.47%



RMSE

24.02%



MAE

28.12%



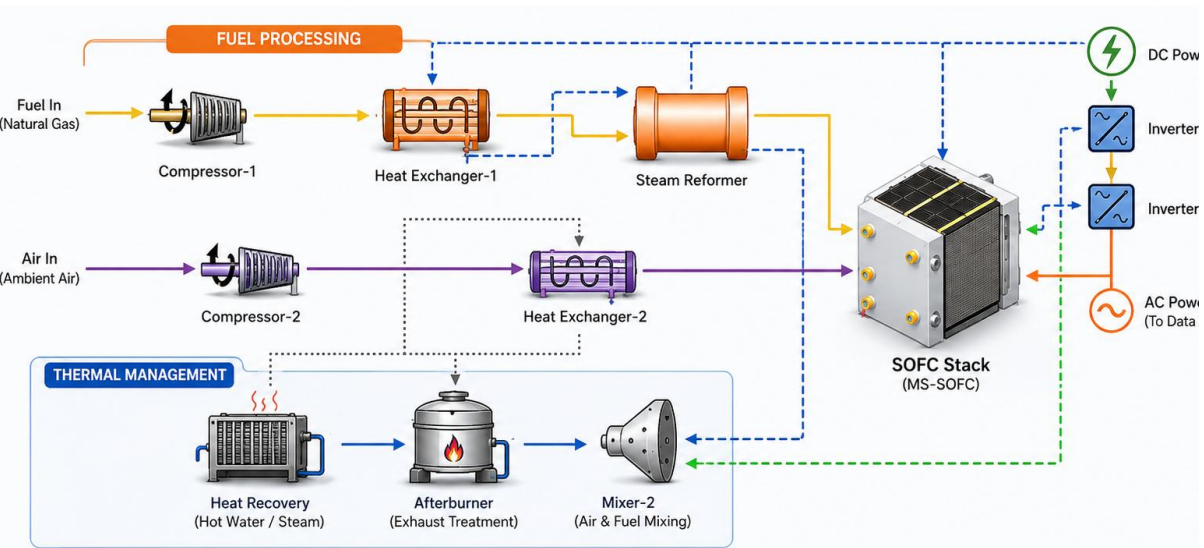
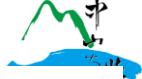
Maximum Absolute Temperature Error

6.86%



Our Team's Research Interests

Metal-Support Solid Oxide Fuel Cell (MS-SOFC)

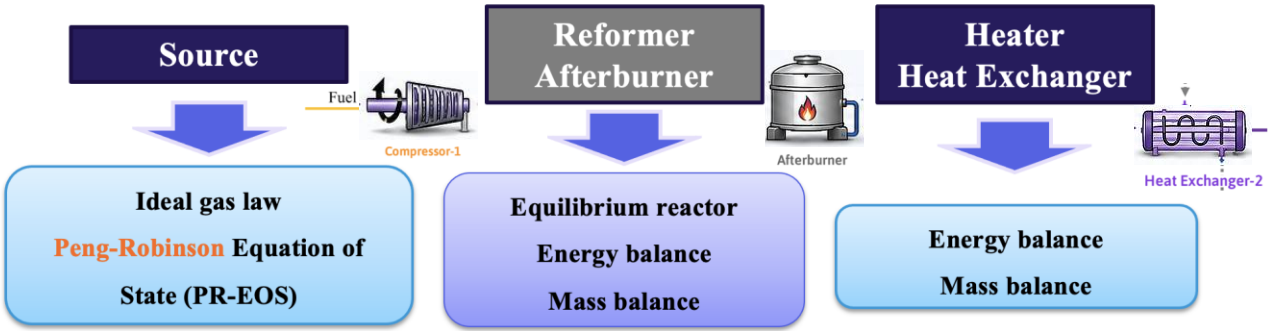


- Mass balances**
1. Fuel Channel
 2. Air Channel
 3. Chemical Reaction

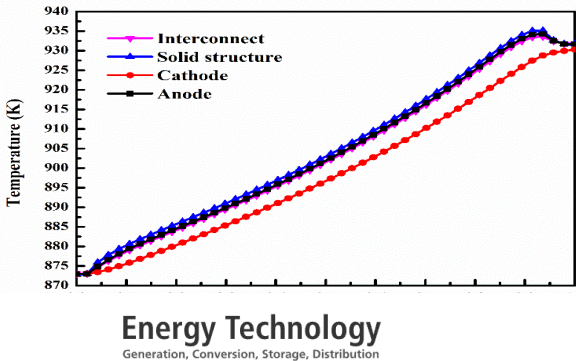
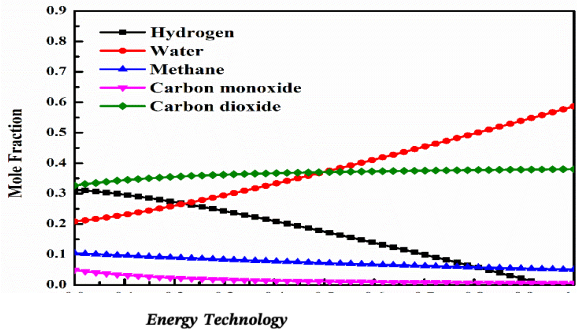
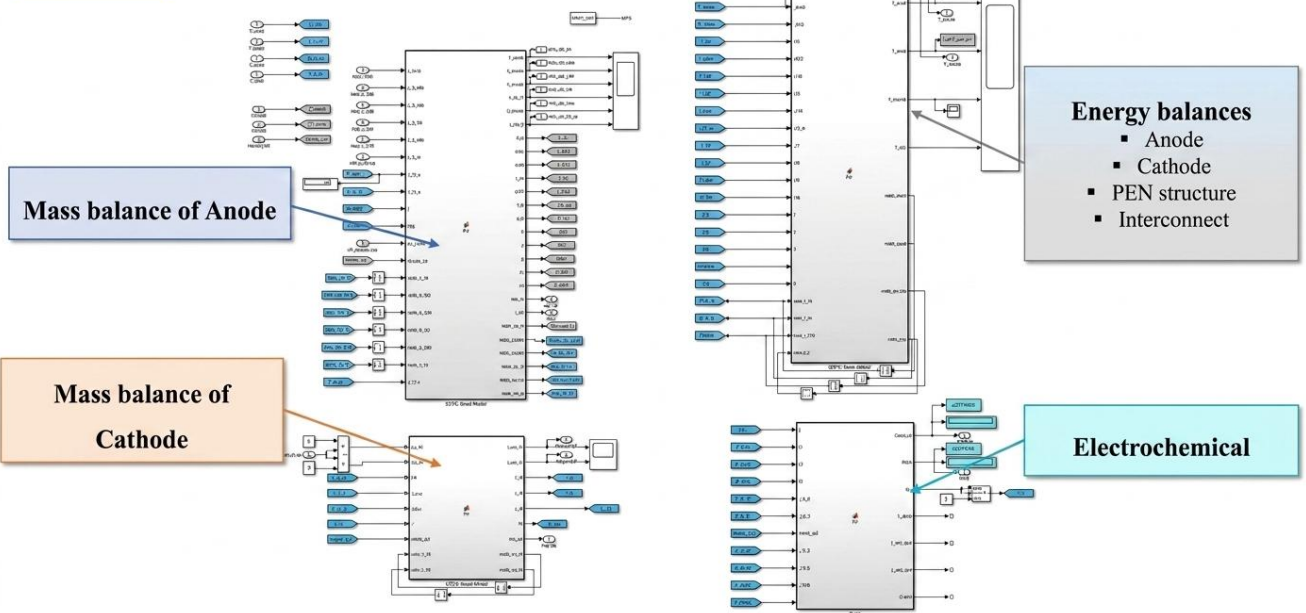
- Energy balances**
1. Fuel Channel
 2. Air Channel
 3. PEN structure
 4. Interconnect

- Electrochemical**
1. Nernst equation
 2. Ohmic Overpotential
 3. Concentration Polarization
 4. Activation loss

Other components



Simulink Modeling MS-SOFC



RESEARCH ARTICLE OPEN ACCESS

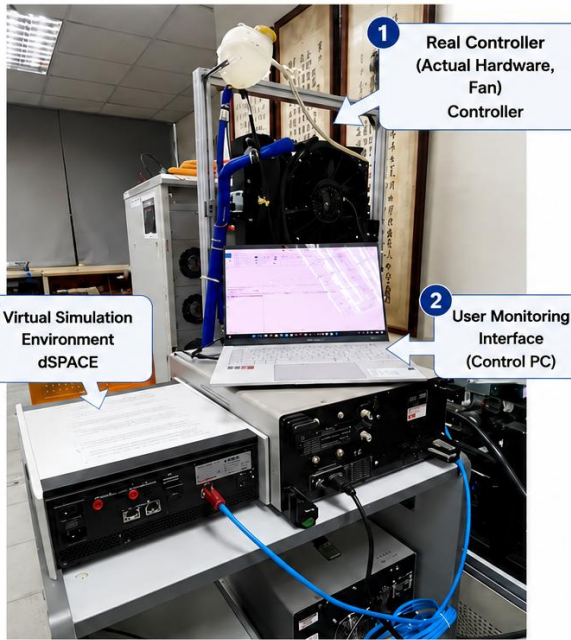
Performance Analysis of Pure Hydrogen and Mixed Fuels in Medium-Temperature Metal-Supported Solid Oxide Fuel Cell

Jenn-Kun Kuo¹ | Ping-Hao Liu¹ | Sen-Wu Chiang² | Wen-Hsin Shen² | Wei-Cheng Wang³

¹Department of Mechanical and Electro-Mechanical Engineering, National Sun Yat-sen University, Kaohsiung, Taiwan | ²Hydrogen Energy Business Development, Delta Electronics, Incorporation, Tainan, Taiwan | ³Department of Aeronautics and Astronautics, National Cheng Kung University, Tainan, Taiwan

HIL (Hardware in the Loop) Test Platform Fuel Cell Thermal System

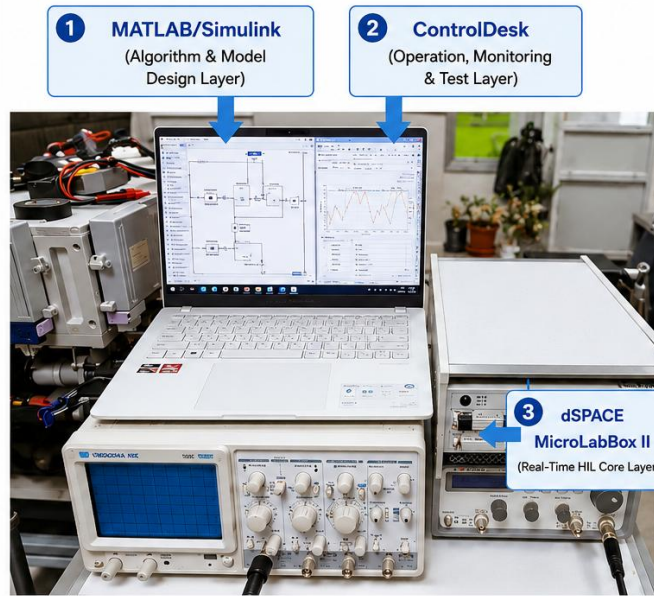
HIL (Hardware-in-the-Loop) Test Platform Experimental Setup



HIL (Hardware-in-the-Loop) Test Platform

Integrates real hardware, dSPACE real-time simulator, and control PC to validate control strategies and system behavior.

HIL (Hardware-in-the-Loop) Test Platform Experimental Setup



HIL (Hardware-in-the-Loop) Test Platform

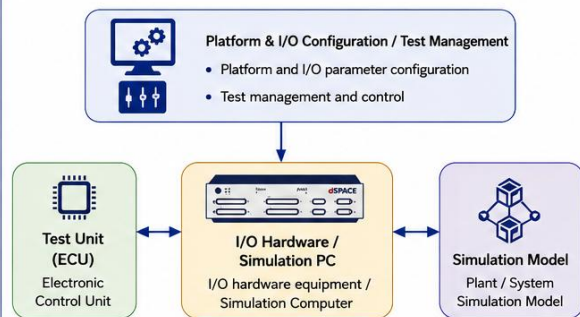
Integrates MATLAB/Simulink, dSPACE MicroLabBox II, and ControlDesk to implement model operation, real-time control, data monitoring, and validation of control strategies and system behavior.

dSPACE MicroLabBox II Hardware / Simulator I/O Interface Configuration



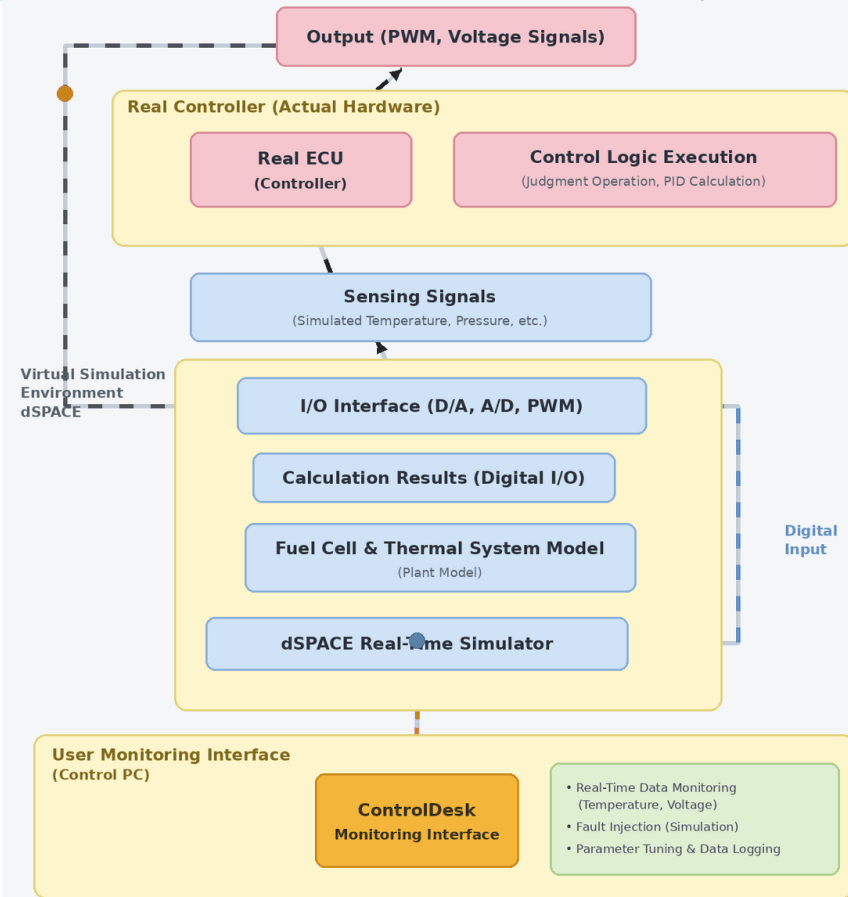
- ✓ High-performance real-time simulator platform
- ✓ Rich I/O interface support
- ✓ Modular design, flexible extension
- ✓ Support multiple communication protocols

(Hardware in Loop, HIL) Hardware-in-the-Loop System Architecture

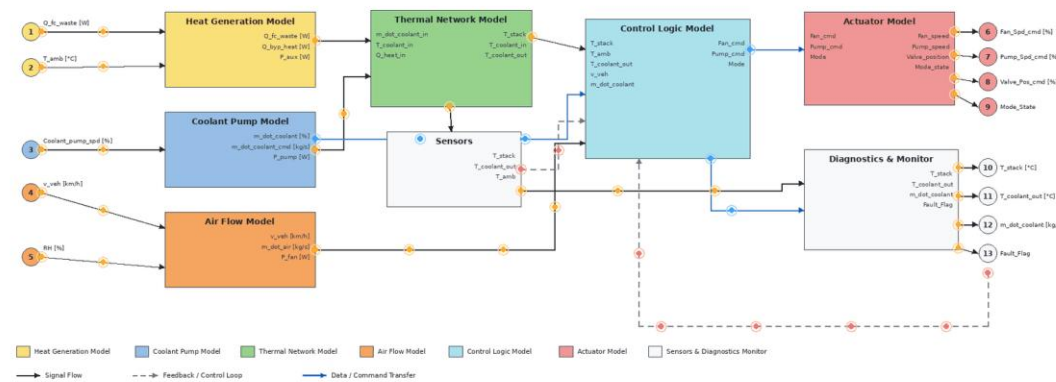


Hardware-in-the-Loop (HIL) Simulation — Signal Flow

Real ECU ↔ dSPACE Virtual Plant (Fuel Cell & Thermal System)

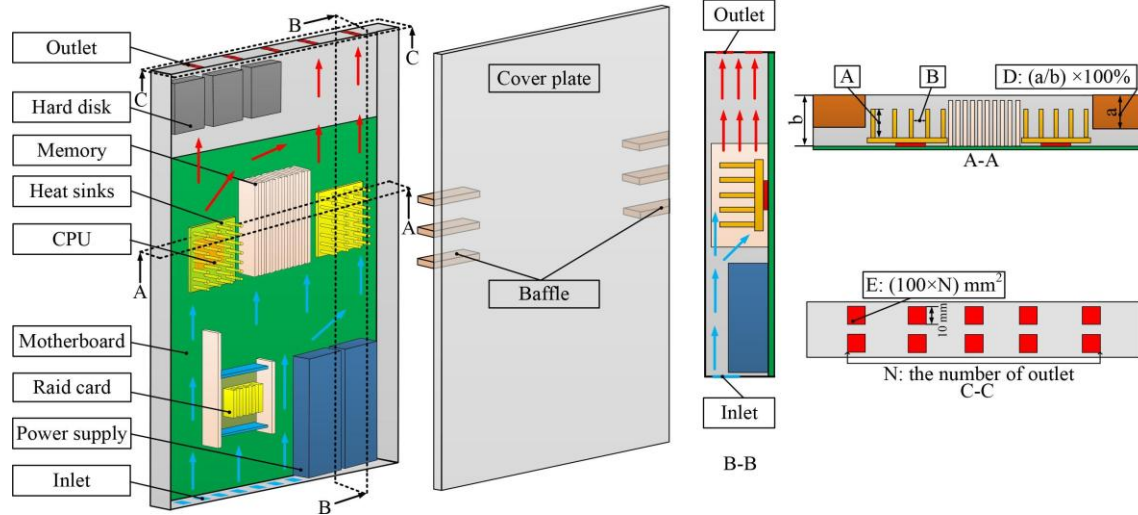


Fuel Cell Thermal Management System Model Diagram

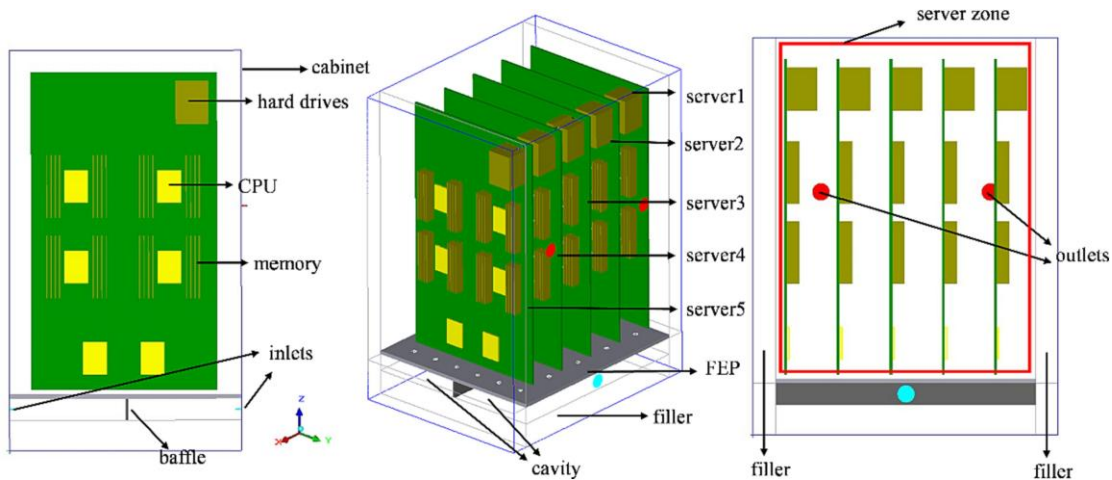


AI Data server's heat transfer

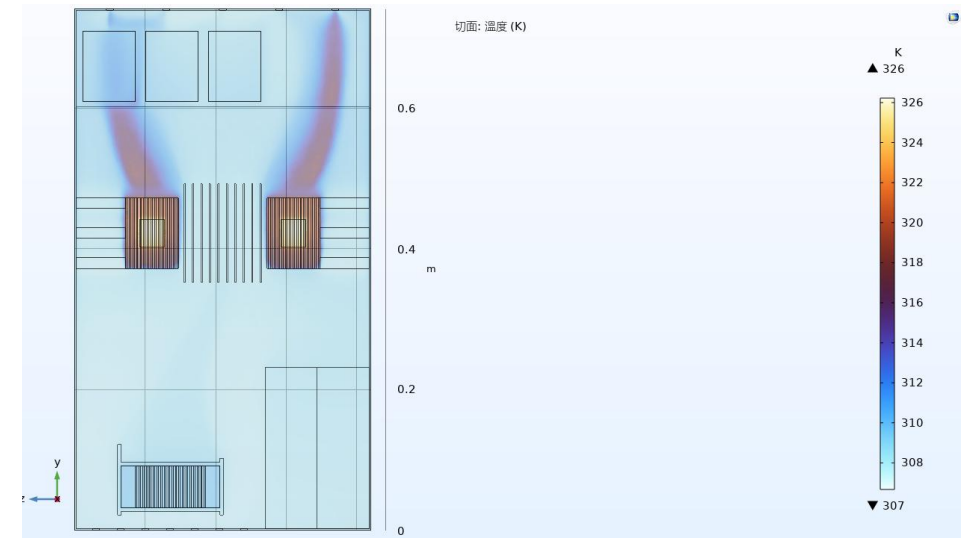
- Computational Fluid Dynamics (CFD)
- Single-Phase Immersion Cooling (SPIC)
- Analysis of Heat Dissipation Performance



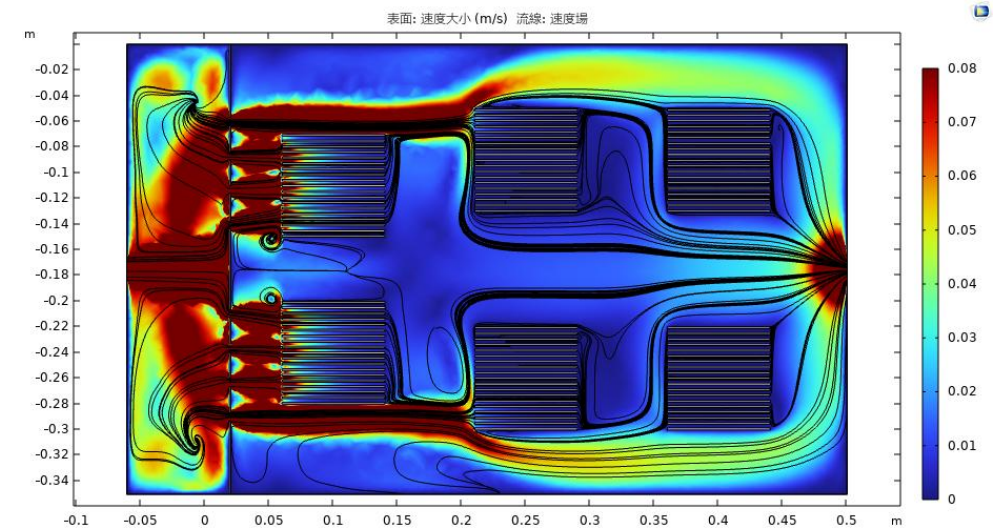
Internal component layout, airflow path, and baffle configuration



Server Cabinet Configuration Adopted from the Literature

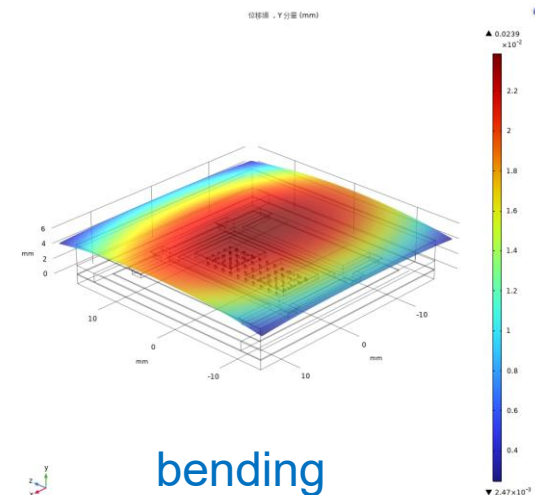
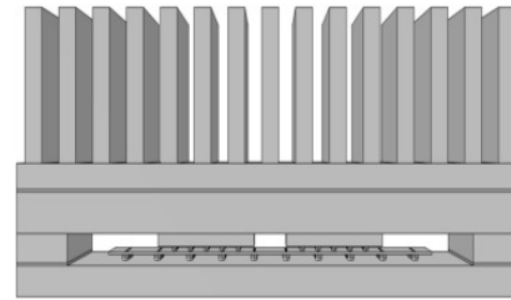
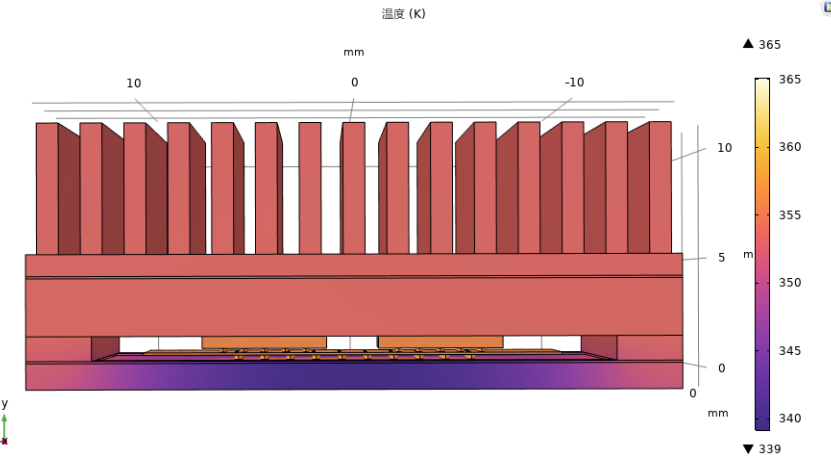
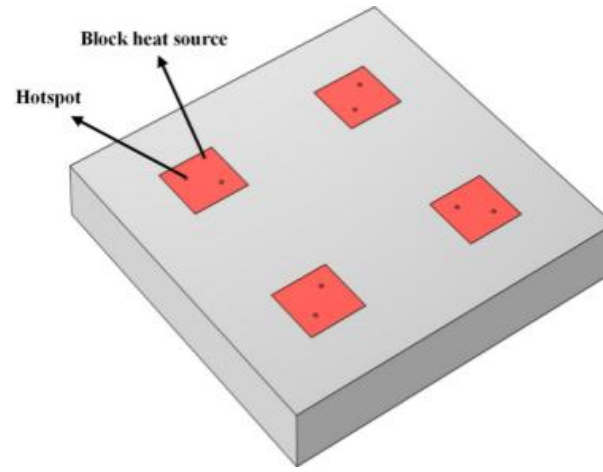
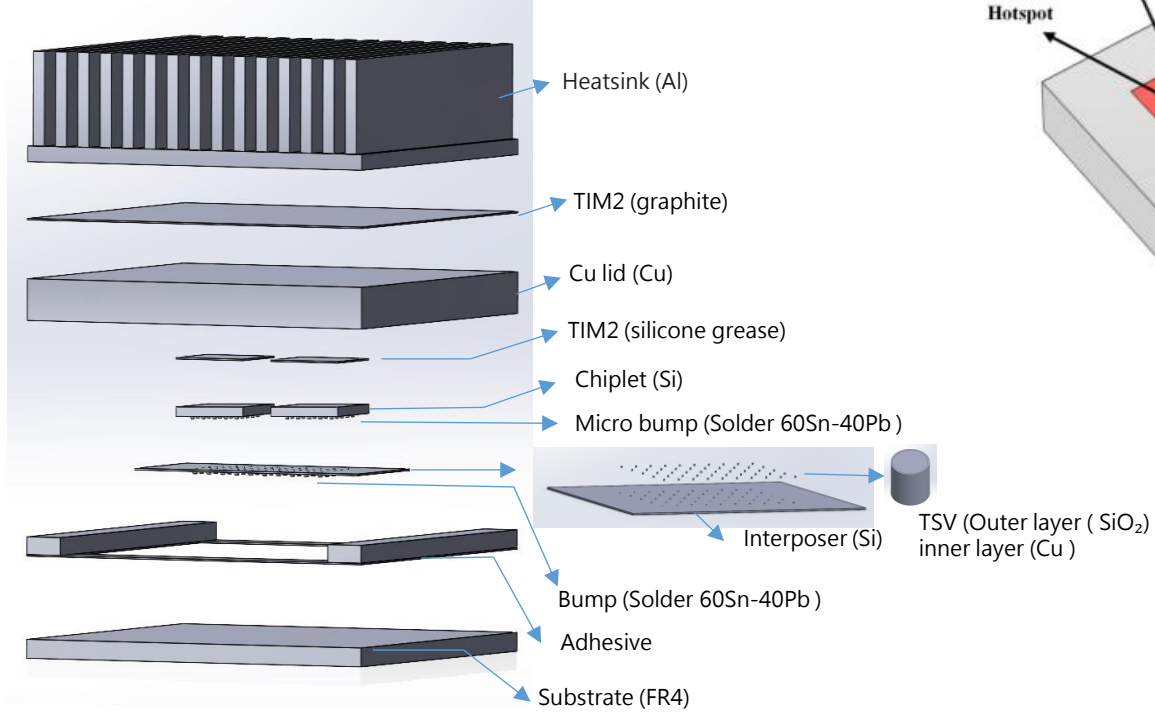


Simulated steady-state temperature distribution

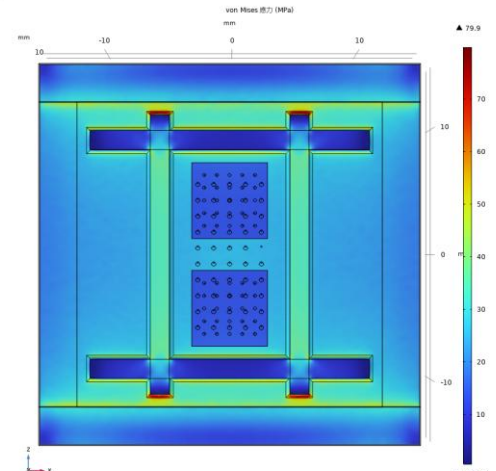
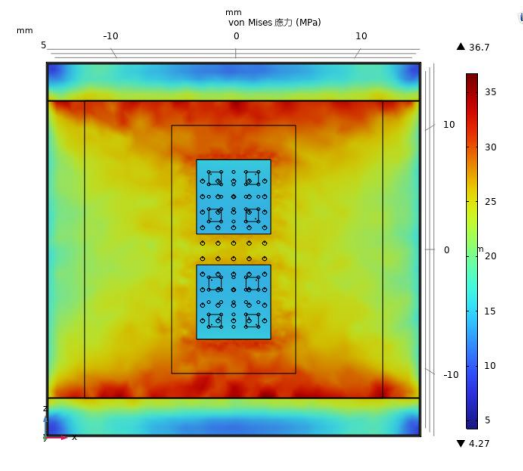


Coolant Velocity Distribution and Flow Streamlines

Semiconductor package structure (ASE Technology Holding Co.)



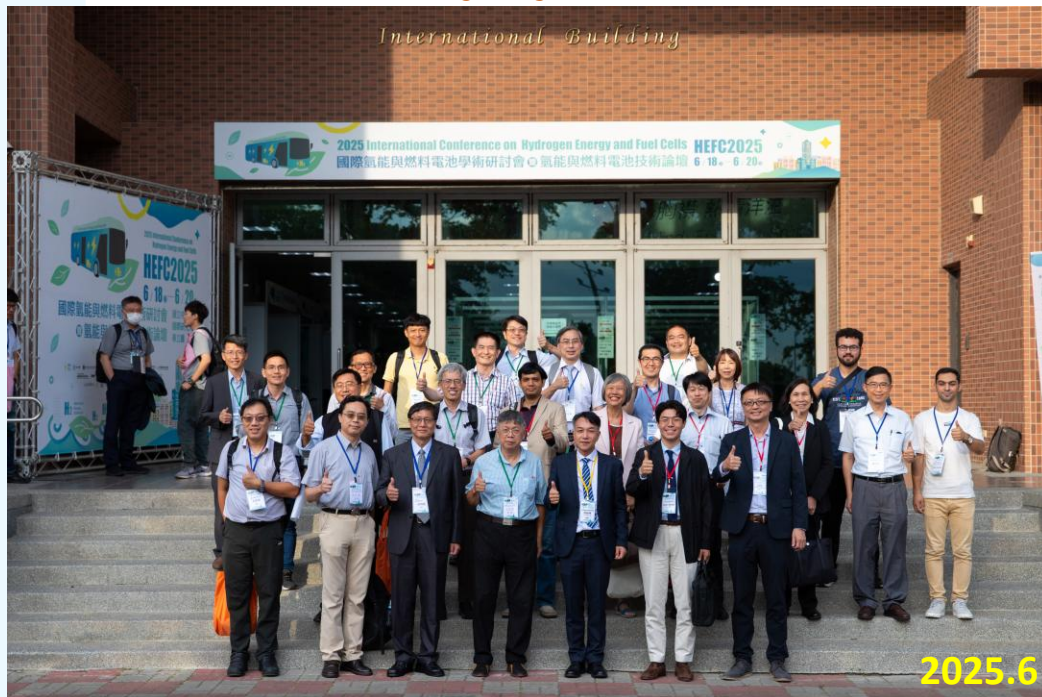
bending



Simulation conditions :

Chiplet spacing	2.5 mm
Bump spacing	1.0 mm
Chiplet Volumetric heat source	2e7 W/m ³
Block heat source	2e5 W/m ²
Hotspot	4e7 W/m ²
Heatsink Surface convection heat transfer coefficient	h = 10 W/m ² K
Substrate Surface convection heat transfer coefficient	h = 2 W/m ² K
Initial/Ambient Temperature	293.15 K

2025 H2 Energy and Fuel Cell Conference in Taiwan



Laboratory Team Members



Thank you for your attention!

Email: jenn.kun@gmail.com